

To: Gerold Noyes Vermont Department of Environmental Conservation Waste Management and Prevention Division Date: 8fUZhApril 18, 2016

Memorandum

Project #: 57603.00

From: Rachel Lomonaco & Meddie J. Perry, CGWP

Re: Middlebury WRCS(23) Bridge Project Pre-Construction Soil and Groundwater Sampling Work Plan

# INTRODUCTION

On behalf of the Vermont Agency of Transportation ("VTrans") and the Town of Middlebury, VHB has prepared this pre-construction soil and groundwater sampling work plan ("Work Plan") for the Middlebury WCRS(23) Bridge Project ("the Project") which includes the full replacement of two roadway bridges in downtown Middlebury where Main Street and Merchants Row span the Vermont Railway, Inc. ("VTR") track. The purpose of the Project is to replace the two bridges with a single tunnel and to depress the VTR track by several feet with excavation required up to approximately 12 feet below existing grade in the area of the current bridges. The track lowering is to comply with federal and state requirements to accommodate taller freight traffic along the VTR track.

This work plan provides protocols for a pre-construction characterization of the Project area to investigate the condition of soil and groundwater that are expected to be encountered within the Project area during Project construction. Specifically, the work plan provides a review of the history of the Project area with respect to contaminants of concern, and outlines procedures to complete soil and groundwater sampling and analysis of contaminants of concern. The results of this investigation will serve to advise VTrans and the Town of Middlebury of design constraints, allowable soil and groundwater handling practices, and disposal requirements for soils and materials that are encountered during Project construction.

# PROJECT AREA

The Project area is located within downtown Middlebury, Vermont to the east of the Otter Creek. A Project Location Map is included on page 1 of the Attachment. Soil Work Plan Engineering Plan sets are included on pages 2-9 of the Attachment. Note that the work plan narrative refers to locations within the Project area in accordance with stationing notation (e.g., 10+00) as defined in the Soil Work Plan Engineering Plan sets.

The Project limits include approximately 3,575 feet of the State right-of-way ("ROW") from the railroad bridge over the Otter Creek (southern limit; Station 10+00) to just north of the Elm Street Bridge (northern limit; Station 45+75). The Project area also includes the Town of Middlebury road ROWs, which are elevated above the VTR track, and includes Main Street from the Merchants Row intersection to Seymour Street and Merchants Row from the Main Street intersection to South Pleasant Street. Additionally, the Project area includes a portion of Triangle Park and areas to the south of Merchants Row, between the VTR track and the bank of the Otter Creek, and an access road to the VTR track off of the western end of Water Street. Lastly, the Project area includes areas to the north of Main Street, in the former location of the Lazarus building (20 Main Street, Middlebury, VT) and an existing underground stormwater pipe and outfall which outlets to the Otter Creek.

Based on a preliminary geotechnical assessment completed by Otter Creek Engineering ("OCE"), the railroad alignment consists of ballast from approximately 0-2 feet below current grade that is partially or completely entrained in soil (OCE, 2013; OCE, 2014). Below the ballast is fill consisting of silty clay to silty sand, with some gravel and underlain by till. Additionally, according to the geotechnical assessment, exposed bedrock is located near the Main Street Bridge abutment and shallow bedrock has been identified in this area

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from Station 25+75 to Station 28+25. Reportedly, bedrock is composed of moderately hard limestone, marble and phyllite (GeoDesign, 2014). According to this geotechnical assessment, Main Street and Merchants Row are composed of several inches of asphalt, underlain by several feet of fill generally consisting of silt, sand and gravel (GeoDesign, 2013). Coal and brick fragments have been noted in fill below Main Street and Merchants Row (GeoDesign, 2013).

Groundwater has been found to be flowing to the west, toward the Otter Creek, and water table elevations are relatively shallow, generally between 1 and 9 feet below existing grade (OCE, 2014; OCE, 2015). Water has been observed to seep from the existing retaining walls north of the Main Street overpass, and surface water runoff from surrounding areas flows downward into the track trough. Water from both of these sources has been reported to pool and collect at the track level, creating icy track conditions in winter months.

# **PROJECT DESCRIPTION**

In general, the Project will involve the replacement of the Merchants Row and Main Street Bridges with a single precast concrete box tunnel. The VTR track will be lowered with excavation below existing grade estimated at approximately 12 feet in the area of the existing bridges, in order to accommodate the new tunnel structure. Grade along the railroad track, to the north and south of the tunnel will be lowered to accommodate a maximum 1% grade as required for railroad design. U-shaped concrete retaining walls ("U-walls"), retaining walls, and/or sheet pile walls, will be placed on either end of the tunnel to stabilize track side slopes.

Stormwater underdrains will be located within the concrete tunnel and concrete U-walls (Station 20+00 to Station 37+50) to accommodate stormwater flow through these areas. Within tunnel and U-wall areas, the stormwater system is designed to be separated from the water table with pre-cast concrete units where the joints are designed to be water tight. These drains will discharge to the bank of the Otter Creek, via an existing outfall at Station 27+25 (a stormwater discharge permit is being sought from the VT DEC). To the south of the tunnel and U-wall areas (Station 10+00 to Station 20+00), stormwater swales will be located on the east and west sides of the track. These swales will be pitched to one of two existing outfalls on the Otter Creek (Station 15+25 and Station 27+25) via above ground swales and/or underground pipes). From the northern limit of the tunnel and U-wall to the Elm Street Bridge (Station 37+50 to Station 42+00) stormwater swales will be located on the east and west sides of the tracks. These swales will be pitched toward catch basins on the east and west side of the tracks at Station 37+60 and stormwater will be diverted west and north to the Town's stormwater system along Elm Street via underground piping. North of the Elm Street Bridge (Station 42+00 to Station 45+75) no drainage structures will be installed.

The Project will involve the disturbance of soil and possibly groundwater in the following portions of the construction area:

- <u>Temporary Access Road</u>: The temporary access road is proposed to be located to the east of the VTR track from Station 10+00 to Station 14+00, crossing the track at Station 14+00, and continuing to the west of the VTR track from Station 14+00 to Station 21+75. Excavation of soil to 1 foot below ground surface ("bgs") is anticipated, to install new gravel subbase and asphalt surfacing. Approximately 400 cubic yards (650 tons) of material is expected to be generated from this excavation. A typical section of the temporary access road construction is included on page 10 of the Attachment.
- 2. <u>Drainage Structures</u>: Stormwater drainage infrastructure construction will include installing new storm drains and service lines along the upgraded railroad tracks. The new storm drains will be connected to an existing outfall located to the north of Main Street, along the bank of the Otter Creek. Storm drain connections will be completed using jack-and-bore type

drilling with a 60 inch horizontal borehole through subsurface bedrock. The drill launch and receiving pits will be constructed as follows:

- Launch Pit (Station 27+25): Excavation will be approximately 20 feet by 30 feet by 45 feet deep, with approximately 12 feet to the bedrock interface. Approximately 270 cubic yards (440 tons) of material is expected to be generated from the Launch Pit excavation.
- b. Drive #1 Receiving Pit (Otter Creek Outfall): Excavation approximately 10 feet by 20 feet by 5 feet deep. Approximately 40 cubic yards (65 tons) of material is expected to be generated from this excavation.
- c. Drive #2 Receiving Pit (Station 25+37): Excavation approximately 15 feet by 15 feet by 45 feet deep. Approximately 35 feet to the bedrock interface. Approximately 300 cubic yards (490 tons) of material is expected to be generated from this excavation.
- d. Drive #3 Receiving Pit (Station 29+00): Excavation approximately 15 feet by 15 feet by 25 feet deep. Approximately 15 feet to the bedrock interface. Approximately 125 cubic yards (200 tons) of material is expected to be generated from this excavation.

Drainage profiles for each of the launch/receiving pits and connecting structures are included on pages 11-13 of the Attachment.

- 3. <u>Railroad Track</u>: Soil will be excavated to a maximum of 12 feet below existing grade under the existing bridges. Excavation of the track is required between from the railroad bridge over the Otter Creek (southern limit, Station 10+00) to just north of the Elm Street Bridge (northern limit, Station 45+75) to accommodate the depression under the existing bridges. U-walls, retaining walls, and sheet pile walls will be installed to the north and south of the tunnel area (Station 16+75 to Station 40+00) for track wall stabilization. Approximately 30,000 cubic yards (49,000 tons) of material is expected to be generated from this excavation. Typical sections of the track reconstruction (sheet piling, U-walls, tunnel, retaining walls and other areas) are included on pages 14-20 of the Attachment.
- 4. <u>Main Street</u>: Excavation of soil within the existing road ROW is required for bridge removal and to accommodate new supportive concrete approach slabs. Excavation of soil to 2 feet below existing grade from Station 200+75 to Station 203+00 excluding the bridge substructure where soils do not exist, and up to 4 feet below existing grade within approximately 25 feet of the existing track retaining walls. Approximately 1,700 cubic yards (2,750 tons) of material is expected to be generated from this excavation. A typical section of the Main Street reconstruction is included on page 21 of the Attachment.
- 5. <u>Merchants Row</u>: Excavation of soil within the existing road ROW is required for bridge removal and to accommodate new supportive concrete approach slabs. Excavation of soil to 2 feet below existing grade from Station 101+75 to Station 104+25, excluding the bridge substructure where soils do not exist, and up to 4 feet below existing grade approximately 25 feet east or west from the existing track retaining walls. Approximately 1,600 cubic yards (2,600 tons) of material is expected to be generated from this excavation. A typical section of the Merchants Row reconstruction is included on page 21 of the Attachment.
- 6. <u>Triangle Park</u>: Excavation of soil within the eastern portion of Triangle Park is required to accommodate the new tunnel and install new track side wall support structures. Excavation of soil to approximately 24 feet below existing grade from Station 24+25 to Station 25+75, including all area within 10-15 feet from the existing western track retaining wall. Approximately 650 cubic yards (1,100 tons) of material is expected to be generated from this excavation.

# **PROJECT AREA HISTORY**

VHB completed a review of available documents to assess the known and potential soil and groundwater conditions within the Project Area. The review included examination of historic Sanborn Maps, a review of the VT DEC Sites Management database and recent geotechnical reports for the Project area for information about subsurface conditions and known contamination.

# Sanborn Map Review

A review of Historic Sanborn Maps (dated 1885, 1892, 1905, 1910, 1920, 1927 and 1944) identifies that the Project area was occupied by a railroad track since at least 1885 in the same general alignment as present-day VTR track. The Main Street and Merchants Row Bridges also existed since at least 1885.

The area between the Otter Creek truss bridge (Station 10+00) and the Cross Street Bridge (Station 15+00) is not shown in the early maps. The 1920, 1927 and 1944 maps extend to this area and depict an ice house and ice storage sheds to the west of the tracks, and a lumber yard and several dwellings to the east of the tracks.

The area to the west of the tracks between the Cross Street Bridge (Station 15+00) and Merchants Row (Station 23+25) contained several storage buildings located near the bank of the Otter Creek (1885 through 1927) and the heating plant for buildings along Merchants Row, consisting of an oil house and gasoline house (1910 through 1944). The area to the east of the tracks historically contained several dwellings. The former Town Hall was located to the east of the tracks, just south of Merchants Row and a gasoline tank is visible to the south of the former Town Hall building in the 1885 and 1892 maps.

The maps indicate that a variety of shops existed along Main Street and Merchants Row in the central Project area, where these streets cross over the VTR track (Station 23+25 to Station 26+50). The former Lazarus Building (Station 27+25) is shown on all of the maps and was occupied by a tailor shop (1885 and 1892), billiards hall (1905), wallpaper and variety store (1910) and unidentified shops (1920, 1927 and 1944). The Lazarus Building was recently demolished.

The area just north of the Main Street Bridge and west of the tracks (Station 29+00 to Station 35+00) was historically occupied by the Marble Works, with several stone cutting and polishing buildings. A coal storage shed was located just west of the tracks (approximately Station in the 30+00) in the 1905, 1910, 1920, 1927 and 1944 maps. The east side of the tracks, in this area, was historically occupied by dwellings.

In the northern portion of the Project area but to the south of the Elm Street Bridge (Station 35+00 to Station 42+00), the surrounding area was historically occupied by dwellings and a railroad passenger depot. In the 1944 map, several buried gasoline tanks were also noted to the east of the tracks, along the east side of the current day Seymour Street (approximately Station 37+50 to Station 40+00) and were associated with historic filling stations.

In the far northern portion of the Project area, to the north of the existing Elm Street Bridge (Station 42+00 to Station 45+75), the areas to the west of the tracks were occupied by residences and the areas to the west were occupied by a railroad yard, consisting of multiple tracks, a freight depot, coal shed, lumber storage and a machine shop. On the 1885, 1892 maps a 46,000 gallon petroleum tank is visible approximately 100 feet east of the Project area. In the 1920, 1927 maps several different oil and gasoline tanks are visible approximately 100 feet to the east of the Project area.

# Train Derailment Investigation

On October 22, 2007 an accidental train derailment occurred between the Otter Creek truss bridge (Station 10+00) and the Merchants Row Bridge (Station 23+25). Reportedly, 25 railcars were derailed, 15 of which contained gasoline and 10 of which contained road salt (OCE, 2008). All the cars overturned to the west of the track, toward the Otter Creek. Reportedly, gasoline leaked from 7 of the 15 overturned railcars and road salt spilled from 4 of the 10 railcars (OCE, 2008). The estimated volume of gasoline released to the environment was between 200 to 1,800 gallons (OCE, 2008). The remainder of the petroleum from the overturned railcars was pumped into truck tankers and hauled off-site. The gasoline spill impacted soil, groundwater, and surface water (Otter Creek) near the derailment area. Additionally, during the derailment, petroleum infiltrated the Town of Middlebury sewer system and was treated at the sewage treatment plant. Sorbent booms were placed in the Otter Creek between October and December 2007. Road salt was manually shoveled out of the derailment area by hand. The Middlebury Train Derailment site was listed by the VT DEC as a hazardous waste site (VT DEC #20093912). In December 2009 and January 2010, injections of chemical oxidants (RegenOx<sup>™</sup> and ORC Advanced®) were completed within the derailment area as a form of groundwater remediation (OCE, 2010).

Two surficial soil samples collected in 2007 (MW-07, -08 and -09) were analyzed for Volatile Organic Compounds ("VOCs") and Total Petroleum Hydrocarbons ("TPH") Gasoline Range Organics ("GRO") and indicated the presence of benzene, toluene, ethylbenzene, xylenes, naphthalene, trimethybenzene, and TPH GRO in excess of the VT DEC residential and industrial Soil Screening Values ("SSVs"). Seven surficial soil samples collected in 2009 (SB-09-01 through -07) were analyzed for TPH GRO and lead, both of which were present at concentrations below the VT DEC residential SSVs (OCE, 2010). PID headspace readings form these 2007 and 2009 soil samples were generally elevated (>100 ppm).

To the west of the VTR track, between the Otter Creek truss bridge and Merchants Row Bridge, 10 groundwater monitoring wells (MW-07-01 through -10) were installed in 2007. Three of these wells (MW-07-03, -04, -05) were destroyed in 2009 during construction of the Cross Street Bridge. One new well was installed in 2009 (MW-09-01) and ten new monitoring (MW-10-01 through -10) wells were installed in 2010. There are currently a total of 18 wells associated with VT DEC #20093912, 13 of which have been recommended for permanent closure. The November 2015 groundwater monitoring data indicates that the Vermont Groundwater Enforcement Standards ("VGES") are exceeded for benzene in four wells (OCE, 2015). Annual groundwater monitoring is ongoing.

# Geotechnical Investigations

In 2013, GeoDesign completed two geotechnical investigations within the Project area. In March 2013, GeoDesign advanced 31 ledge probes, 25 soil borings and 11 test pits. PID headspace readings from soils within the VTR track, Merchants Row, Main Street and behind the eastern retaining wall, north of Main Street, were relatively low (<4 ppm; GeoDesign, 2013). In October/November 2013, GeoDesign completed additional soil borings, ledge probes and rock coring. No PID headspace readings were collected during this assessment (GeoDesign, 2014).

In March 2016, GeoDesign completed seven test pits along the railroad tracks, under the Main Street Bridge. The test pits were advanced to determine the depth to bedrock and depth of pier support structures which support the Main Street Bridge. Test pits indicated that the depth to bedrock varies from approximately 5.4 feet below grade near the southern limit of the Main Street Bridge to approximately 1.4 feet below grade near the northern limit of the Main Street Bridge.

During GeoDesign's March and October/November 2013 geotechnical investigations, eight groundwater wells were installed along the VTR track to monitor the groundwater elevation within the Project area. Each well was installed with 5 or 10 feet of factory slotted screen and was backfilled with clean filter sand to above the well screen, capped with a bentonite plug and backfilled with native materials to the ground surface (GeoDesign, 2013; GeoDesign, 2014). Each well is capped with a PVC expansion plug and finished with a flush mounted road box at ground surface. Well construction details are included in the table below.

Existing Groundwater Monitoring Wells – VTR Track									
Well ID	Station	Well Depth*	Well Screen*	Installation Date					
GBD-2 (OW)	13+75	10	5-10	Oct/Nov2013					
GBD-5 (OW)	18+00	7	3-7	Oct/Nov 2013					
RR-11 (OW)	21+00	10	5-10	March 2013					
RR-13 (OW)	23+00	10	5-10	March 2013					
RR-16 (OW)	25+50	10	5-10	March 2013					
RR-1 (OW)	29+00	10	5-10	March 2013					
GBD-16 (OW)	32+00	15	5-15	Oct/Nov 2013					
GDB-20 (OW)	35+50	30	20-30	Oct/Nov 2013					
*Units in feet below gr	ound surface ("bgs"	).							

Soil boring and well construction logs for the wells listed in the table above are included on pages 36-45 of the Attachment.

# Conceptual Site Model and Evaluation of Contaminants of Concern

The Project area is located in downtown Middlebury, Vermont and generally consists of a railroad track and two elevated roadways. The purpose of the Project is to replace the Main Street and Merchants Row Bridges with a single tunnel and to depress the VTR track by several feet with excavation required as deep as approximately 12 feet below existing grade in the area of the current bridges.

Within the railroad alignment, shallow soils consists of stone ballast entrained in soil from current grade to approximately two feet deep. Below the ballast and outside of the railroad alignment, shallow soils consist of silty clay to silty sand, with some gravel, and are underlain by till. Main Street and Merchants Row consist of several inches of asphalt, underlain by several feet of fill, generally consisting of silt, sand and gravel. Shallow or exposed bedrock is located along the rail road track, near the Main Street Bridge abutment. Groundwater has been found to be flowing to the west, toward the Otter Creek, and water table elevations are relatively shallow.

The following contaminants of concern were identified through a review of historic Sanborn Maps, the VT DEC Sites Management database and recent geotechnical reports for the Project area:

Petroleum-impacted soil and groundwater have been identified and are likely to be encountered in the southern Project area (approximately Station 10+25 to Station 20+00) in association with a 2007 train derailment (VT DEC #20093912).

- The historic site use as a railroad corridor indicates the likelihood of surficial soil contamination within the Project area. Railroad contaminants typically include, but are not limited to, metals (specifically lead and arsenic), PAHs, petroleum compounds, herbicides and pesticides.
- > Surficial soil and shallow groundwater contamination is likely in consideration of the following historic adjoining site uses:
  - o railroad yard and petroleum storage tanks to the east of the tracks at Station 42+00 to Station 45+75,
  - o coal storage shed to the west of the tracks at Station 30+00,
  - o petroleum underground storage tanks to the east of the tracks at Station 37+50 to Station 40+00,
  - o petroleum heating tanks east of the tracks associated with the former Town Hall at Station 20+50, and
  - o petroleum heating tanks west of the tracks associated with the buildings along Merchants Row at Station 22+25

The Otter Creek has been identified as a potential receptor for this Project, although surface water sampling associated with the train derailment (VT DEC #20093912) has indicated that this potential receptor is not currently impacted by the groundwater contamination within the southern Project area. In addition, another potential receptor is a Class II wetland is mapped by the Vermont State Wetland Inventory to the west of the southern Project area, near the Otter Creek. No other wetlands, water bodies, drinking water wells or source protection areas have been identified within the vicinity of the Project area. The surrounding area is supplied with potable water from the municipal system.

The primary concern associated with potential contamination at the Project is the management of contaminated soils that must be excavated for construction, and the need to comply with the applicable regulations for worker exposure, soil placement or stockpiling, and final disposal.

# SOIL SAMPLING WORK PLAN

VHB presents this soil sampling work plan to perform pre-construction site characterization in order to assess the condition of soil within the Project area that may be disturbed as part of Project construction. Based on Project design, a net cut of soil is anticipated from each Project sub-area (temporary access road, drainage structures, railroad track, Main Street and Merchants Row); therefore soil will be characterized based on the contaminants of concern as determined by review of the Project area history, and to determine the appropriate handling practices and disposal requirements, as necessary.

Prior to any drilling or digging, DigSafe will be contacted to mark out underground utilities within the Project area. Drilling will be completed using a Geoprobe rig, or equivalent, by a licensed drilling company. An environmental scientist with OSHA HAZWOPER certification and appropriate field training will observe the drilling, log soils, and will use a photoionization detector ("PID") with a properly calibrated 11.2 eV lamp to screen soil for contamination. Soil screening will be completed in accordance with VHB's field screening standard operating procedure included on pages 22-24 of the Attachment.

Soil borings will be advanced within the Project area and soil sampling will be completed as follows:

	Soil Sampling Summary							
Project Sub-area	General Notes	Soil Boring Stations	Sampling Depth					
Temporary Access	One soil boring every 100 feet of	Stations: 11+75, 12+75, 13+75,	1ft bgs					
Road	roadway. Soil borings will be advanced to	14+75, 15+75, 16+75, 17+75,						
	proposed construction depths (1ft bgs).	18+75, 19+75 and 20+75.						
Drainage	One soil boring from each launch and	Station 25+37	2ft bgs and bedrock					
Structures	receiving pit. Soil borings will be	(Receiving Pit #2)	interface.					
	advanced to proposed construction	Station 27+25	2ft bgs and bedrock					
	depths or to bedrock, whichever is	(Launch Pit)	interface.					
	shallower.	Station 29+25	2ft bgs and bedrock					
		(Receiving Pit #3)	interface.					
		Otter Creek Outfall	2ft bgs and proposed					
		(Receiving Pit #1)	construction depths or to					
			bedrock, whichever is					
		· · · · · · · · · · · · · · · · · · ·	shallower.					
Railroad Track	One soil boring every 50 feet of track.	Stations: 10+00 to 15+00	2ft bgs					
	Soil borings will be advanced to	(every 50 feet)						
	proposed construction depths or to	Stations: 15+50 to 20+50	2ft and 6ft bgs					
	bedrock, whichever is shallower.	(every 50 feet)						
		Stations: 21+00 to 25+00	2ft, 6ft and 12ft bgs					
		(every 50 feet)						
		Stations: 25+50 to 28+00	2ft bgs, or bedrock interface					
		(every 50 feet)						
		Stations: 28+50 to 38+00	2ft and 6ft bgs					
		(every 50 feet)						
		Stations: 38+50 to 45+50	2ft bgs					
		(every 50 feet, except Station						
	·	42+00 where a railroad bridge						
		is located over Elm Street)						
Main Street	One soil boring every 50 feet of roadway.	Stations: 102+00, 102+50,	2ft bgs					
	Soil borings will be advanced to	103+00, 103+50, 104+00.						
	proposed construction depths.							
Merchants Row	One soil boring every 50 feet of roadway.	Stations: 201+00, 201+50,	2ft bgs					
	Soil borings will be advanced to	202+00, 202+50, 203+00.						
	proposed construction depths.							
Triangle Park	One soil boring every 50 feet of park, to	Stations: 24+75, 25+25	2ft and 24ft bgs					
	be disturbed. Soil borings will be	10-15 feet east of the existing						
	advanced to proposed construction depths.	track retaining wall.						

Proposed soil boring locations are depicted on the Soil Work Plan Engineering Plans on page 2-9 of the Attachment.

Soil samples will be collected in accordance with VHB's soil collection standard operating procedure included on pages 25-28 of the Attachment. All soil samples will be preserved on ice and delivered to a certified testing laboratory, under a chain of custody. Soil samples will be submitted for the following laboratory analysis:

- VOCs via EPA 8260
- > Semi Volatile Organic Compounds ("SVOC") via EPA 8270
- > RCRA 8 metals by various analytical methods
- > TPH GRO and Diesel Range Organics ("DRO") via EPA method 8015
- > PCBs by EPA method 8082
- Pesticides via EPA method 8080
- Herbicides via EPA method 8151A
- Corrosivity
- > Reactivity
- Ignitability

# **GROUNDWATER SAMPLING WORK PLAN**

VHB presents this groundwater sampling work plan perform pre-construction site characterization in order to assess the condition of groundwater within the Project area that may be encountered or disturbed as part of Project construction. Based on Project design, and the expected depth to groundwater, it is likely that groundwater would infiltrate excavation areas. Therefore, the condition of groundwater will be assessed using existing monitoring wells and proposed new monitoring wells to determine the appropriate handling practices and disposal requirements, as necessary.

As previously discussed, an established array of groundwater monitoring wells associated with VT DEC #20093912 exists along the VTR track; therefore, no additional groundwater wells are proposed to be installed in association with the VTR track. However, no groundwater wells are located near the drainage structures, therefore groundwater monitoring wells will be installed in each of the drainage structures launch and receiving pits, generally terminating at proposed construction depths or bedrock, whichever is shallower. Depending on depth, five or ten feet of factory slotted screen will be installed in the bottom of the well, with solid riser to ground surface. The well annulus will be filled with clean filter sand to above the well screen, capped with a bentonite plug and backfilled with native materials to ground surface. A steel flush-mounted well box will be installed at ground surface and the well casing will be capped with a PVC expansion plug. Prior to any drilling or well installations, DigSafe will mark out underground utilities nearby the proposed drilling areas. Drilling will be completed using a Geoprobe rig, or equivalent, by a licensed drilling company.

Groundwater wells will be installed within the Drainage Structure launch/receiving pit footprints and groundwater sampling will be completed using these new and existing wells as follows:

Groundwater Sampling Summary						
Project Sub-area	General Notes	Well Stations	Sampling Methods			
Drainage	Install one overburden well in each of the	Station 25+37	Low flow purge procedures.			
Structures	launch/receiving pits, generally	(Receiving Pit #2)				
	terminating at proposed construction	Station 27+25				
	depths or bedrock, whichever is	(Launch Pit)				
	shallower. Sample groundwater within	Station 29+00				
	these newly installed wells.	(Receiving Pit #3)				
		Otter Creek Outfall				
		(Receiving Pit #1)				
Railroad Track	Sample groundwater within these	Station 13+75	Low flow purge procedures.			
	existing wells which were previously	GBD-2(OW)				
	installed along the VTR track by	Station 18+00				
	GeoDesign in 2013.	GBD-5(OW)				
		Station 21+00				
		RR-11(OW)				
		Station 23+00				
		RR-13(OW)				
		Station 25+25				
		RR-16(OW)				
		Station 29+00				
		RR-1(OW)				
		Station 32+00				
		GBD-16(OW)				
		Station 35+50				
		GDB-20(OW)				

Proposed groundwater well locations are included in the Soil Work Plan Engineering Plans on pages 2-9 of the Attachment.

Each well will be sampled using a peristaltic pump, and disposable dedicated tubing using standard low-flow purge procedures. Groundwater samples will be collected in accordance with VHB's low flow groundwater collection standard operating procedure included on pages 29-35 of the Attachment. All groundwater samples will be preserved on ice and delivered to a certified testing laboratory, under a chain of custody. Groundwater samples will be submitted for the following laboratory analysis:

> VOCs via EPA 8260

# **SCHEDULE**

The Project team will initiate the proposed pre-construction in-situ characterization as soon as possible upon receipt of written work plan approval by the VT DEC. VHB's goal is to commence soil borings and monitoring well installation during the spring of 2016 because construction of the temporary access road and drainage structures is anticipated for the 2016 construction season and is planned to be bid as a VTrans early release package. Construction of the railroad track and bridges is anticipated for the 2017 or 2018

construction season and is planned to be bid as a VTrans construction release package. Therefore, characterization of soil and groundwater within the temporary access road and drainage structures will be prioritized to maintain the current construction schedule and may occur prior to characterization in the railroad track, Main Street or Merchants Row.

Results will be reported to the VT DEC within approximately 60 days from the receipt of laboratory results unless the results indicate a new release which would be reported to the VT DEC as soon as possible. VHB anticipates submitting two follow up reports for the Project; one report for the early release bid package and one report for the construction release bid package. The reports will contain, soil boring logs, tabulated data, laboratory analytical reports and a narrative presenting a sensitive receptor survey, and VHB's findings and recommendations for contaminated media management and disposal options.

# **ATTACHMENTS**

Page 1:	Location Map
Pages 2-9:	Soil Work Plan Engineering Plan (sheet 1-8)
Page 10:	Temporary Access Road Section
Pages 11-13:	Drainage Structure Profiles
Pages 14-20:	Typical Railroad Sections
Page 21:	Main Street & Merchants Row Sections
Pages 22-24:	PID Soil Screening SOP
Pages 25-28:	Soil Sampling SOP
Pages 29-35:	Low-flow Groundwater Sampling SOP
Pages 36-45:	Well logs GeoDesign 2013 wells

# **REFERENCES**

- (OCE, 2008), Otter Creek Engineering, Inc., "Vermont Railway, Inc. Middlebury Train Derailment, Middlebury, Vermont, Subsurface Investigation Report." September 2008.
- (OCE, 2010), Otter Creek Engineering, Inc., "Vermont Railway, Inc. Middlebury Train Derailment (Site #2009-3912), Middlebury, Vermont, Remediation Assessment Report." June 2011.
- (OCE, 2014), Otter Creek Engineering, Inc., "Vermont Railway, Inc. Middlebury Train Derailment (Site #2009-3912), Middlebury, Vermont, Monitor and Water Quality Report December 2014." January 2015.
- (OCE, 2015), Otter Creek Engineering, Inc., "Vermont Railway, Inc. Middlebury Train Derailment (Site #2009-3912), Middlebury, Vermont, Monitor and Water Quality Report November 2015." April 2016.
- (GeoDesign, 2013), GeoDesign, Inc. "Phase A Geotechnical Data Report, Middlebury WRCS(23), Bridge No. 2 and 102 over the Vermont Railway, Middlebury, VT." May 14, 2013.
- (GeoDesign, 2014), GeoDesign, Inc. "Phase B Geotechnical Data Report, Middlebury WRCS(23), Main St Bridge No. 102 and Merchants Row Bridge No. 2 over the Vermont Railway, Middlebury, VT." January 10, 2014.

# ATTACHMENT





LEGEND: = SOIL SAMPLE 2FT BELOW GRADE (RAILROAD TRACK) = SOIL SAMPLE 2FT AND 6FT BELOW GRADE (RAILROAD TRACK) = SOILS SAMPLE 2FT, 6FT, 12FT BELOW GRADE (RAILROAD TRACK) SOIL SAMPLE 2FT BELOW GRADE AND BEDROCK INTERFACE (DRAINAGE STRUCTURES) SOIL SAMPLE 2FT BELOW GRADE (MAIN ST. AND MECHANTS ROW) SOIL SAMPLE IFT BELOW GRADE (TEMPORARY ACCESS ROAD) = APPROXIMATE LOCATION OF EXISTING GROUNDWATER MONITORING WELLS

 $\sum z Z$ VT STATE PLANE GRID











= SOIL SAMPLE 2FT BELOW GRADE AND BEDROCK INTERFACE (DRAINAGE STRUCTURES) = SOIL SAMPLE 2FT BELOW GRADE (MAIN ST. AND MECHANTS ROW) = SOIL SAMPLE IFT BELOW GRADE (TEMPORARY ACCESS ROAD) = EXISTING GROUNDWATER MONITORING WELLS

SOUTH PLEASANT STREET









project name: MIDDLEBU	RY
PROJECT NUMBER: WCRS(23)	
FILE NAME: zIOg044nul_Soil-Charac PROJECT LEADER: M.A. COLGAN DESIGNED BY: R. LOMONACO SOIL WORK PLAN (5 OF 8)	terization DATE: 2/19/2016 DRAWN BY: M.F.SUFFEL CHECKED BY:VHB SHEET 5 OF 8
	PROJECT NAME: MIDDLEBU PROJECT NUMBER: WCRS(23) FILE NAME: ZIOgO44nul_Soil-Charac PROJECT LEADER: M.A. COLGAN DESIGNED BY: R. LOMONACO SOIL WORK PLAN (5 OF 8)



	PROJECT NAME: MIDDLEBURY PROJECT NUMBER: WCRS(23)	
vhb	FILE NAME: zIOgO44nul_Soil-Characterizat PROJECT LEADER: M.A.COLGAN DESIGNED BY: R.LOMONACO SOIL WORK PLAN (6 OF 8)	ionPloOgT DATE: 2/19/2016 DRAWN BY: M.F. SUFFEL CHECKED BY: R. LOMONACO SHEET 6 OF 8
		VHB 57603

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TO NEW HAVEN

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	PROJECT NAME: MID PROJECT NUMBER: WC	DLEBURY RS(23)		
hb	FILE NAME: zIOgO44nul_Sc PROJECT LEADER: M.A.CO DESIGNED BY: R.LOMO SOIL WORK PLAN (7 OF 8	JI-Characterizatio LGAN NACO	DRAWN BY: DRAWN BY: CHECKED BY: SHEET 7	2/19/2016 M.F. SUFFEL R. LOMONACO OF 8







TO NEW HAVEN

	PROJECT NAME: PROJECT NUMBER:	MIDDLEBURY WCRS(23)					
)	FILE NAME: ZIOGO44 PROJECT LEADER: M DESIGNED BY: F SOIL WORK PLAN (8	nul_Soil-Characterizatio M.A.COLGAN R.LOMONACO OF 8)	mPlic@gTh DAT DRAWN BY CHECKED E SHEET	E: : 3Y: 8	2/19/2 M.F. SL R. LOM OF	OI6 JFFEL ONACO 8	



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ITEM 528.11.

MIDDLEBURY PROJECT NAME: PROJECT NUMBER: WCRS(23) ATE: 10/20/2015 BY: E.A. FIALA BY: VHB

I. ALL WORK ASSOCIATED WITH THE INSTALLATION AND REMOVAL OF MAIN ST TEMPORARY ROAD WILL BE

TEMPORARY CONCRETE BLOCKS OR RETAINING

INCLUDED IN THE UNIT PRICE BID FOR CONTRACT

STRUCTURES TO BE DESIGNED AND DETAILED WITH ADDITIONAL CMGC INPUT DURING FINAL DESIGN.

INCLUDED IN THE UNIT PRICE BID FOR CONTRACT ITEM 900.645, "SPECIAL PROVISION (TEMPORARY ACCESS ROAD)".

3. ALL WORK ASSOCIATED WITH THE INSTALLATION AND REMOVAL OF THE TEMPORARY ACCESS ROAD WILL BE

FILE NAME: zI0g044typ.dgn	PLOT DA
PROJECT LEADER: M.A. COLGAN	DRAWN B
DESIGNED BY: E.A. FIALA	CHECKED
TYPICAL ROADWAY SECTIONS (4 OF 5)	SHEET

13 OF 158

VHB 57603

-EXISTING GROUND

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RATINAGE OUTLET PROFIL MICROTUNNEL DRIVE NO. I STA. 0+50 - 2+25 SCALE I'' = 20' HORIZONTAL I'' = 10' VERTICAL

	PROJECT NAME: MIDDLEBURY PROJECT NUMBER: WCRS(23)	
hb	FILE NAME: zIOg044pro_Utilities.dgn PROJECT LEADER: M.A. COLGAN DESIGNED BY: J.D. TREARCHIS DRAINAGE OUTLET PROFILE	PLOT DATE: 10/20/2015 DRAWN BY: A.J. GOUDREAU CHECKED BY: T.M. GINGRAS SHEET 63 OF 158





SCALE I'' = 20' HORIZONTAL I'' = 10' VERTICAL

APPROX	ΙΜΑΤΕ	TOP	OF R	OCK F	PROFILE	BASED
ON G	EOTECH	INICA	L INS	SPEC	TION DA	TA FOR
- ROCK	WITHI	N CE	NTER	OF F	RAILROA	d line

	project name: MIDDLE	EBURY					
	PROJECT NUMBER: WCRS(	23)					
	FILE NAME: z10g044pro_Utiliti	es₁dgn	PLOT DA	TE: IC	0/20/2	2015	
	PROJECT LEADER: M.A. COLGAN	I	DRAWN B	Y: P	.A. MIL	LER	
10	DESIGNED BY: J.D. TREARC	HIS	CHECKED	BY: T	.M. GIN	GRAS	
	MICROTUNNEL DRIVE NO. 2 PRO	FILE SHEET	SHEET	64	OF I	58	



MICROTUNNEL DRIVE NO. 3 STA. 100+50 - 102+50 SCALE I'' = 20' HORIZONTAL I'' = 10' VERTICAL



	PROJECT NAME: MIDDLEBURY PROJECT NUMBER: WCRS(23)	
hb	FILE NAME: zIOgO44pro_Utilities.dgn PROJECT LEADER: M.A. COLGAN DESIGNED BY: J.D. TREARCHIS MICROTUNNEL DRIVE NO.3 PROFILE SHEET	PLOT DATE: IO/2O/2OI5 DRAWN BY: P.A. MILLER CHECKED BY: T.M. GINGRAS SHEET 65 OF I58

I'-O" STONE FILL, TYPE I-GEOTEXTILE UNDER STONE FILL-DRAINAGE AGGREGATE (TYP)-I2" PERFORATED UNDERDRAIN (TYP)——/ EXISTING GROUND-MA+, I'-O" STONE FILL, TYPE I GEOTEXTILE UNDER STONE FILL











![](_page_28_Figure_0.jpeg)

MIDDLEBURY PROJECT NUMBER: WCRS(23) FILE NAME: zI0g044typ.dgn PLOT DATE: 10/20/2015 PROJECT LEADER: M.A. COLGAN DRAWN BY: E.A. FIALA DESIGNED BY: HMM/VHB CHECKED BY: M.A. COLGAN

TYPICAL RAIL SECTION (4 OF 7)

![](_page_28_Picture_4.jpeg)

SHEET 6 OF 158

![](_page_29_Figure_0.jpeg)

-WATERPOOFING MEMBRANE, COSTS SHALL BE INCIDENTAL TO PRECAST CONCRETE STRUCTURE (TUNNEL)

	PROJECT NAME: MIDDLEBURY PROJECT NUMBER: WCRS(23)	
vhb	FILE NAME: zIOg044typ.dgn PROJECT LEADER: M.A. COLGAN DESIGNED BY: HMM/VHB TYPICAL RAIL SECTION (5 OF 7)	PLOT DATE: 10/20/2015 DRAWN BY: K.C. BARRY CHECKED BY: M.A. COLGAN SHEET 7 OF 158

![](_page_30_Figure_0.jpeg)

ETE TOP	TUNNEL	SECTION			
	_\\/.		\//	\//	

- GRANULAR BACKFILL FOR STRUCTURES (TYP)

-BEDROCK (ELEVATION VARIES)

	PROJECT NAME:	MIDDLEBURY	
	PROJECT NUMBER:	WCRS(23)	
-	FILE NAME: ZIOg044	typ.dgn	PLOT DATE: 10/20/2015
b	DESIGNED BY: H TYPICAL RAIL SECT	MACOLGAN IMM/VHB ION (6 OF 7)	DRAWN BY: E.A. FIALA CHECKED BY: M.A. COLGAN SHEET 8 OF 158

![](_page_31_Figure_0.jpeg)

NOTE: RAILROAD ROW VARIES AND IS NOT SHOWN.

TYPICAL RETAINING WALL SECTION STA. 37+50 - 40+00 SCALE 1/2 " = 1'-0"

![](_page_31_Picture_3.jpeg)

- EXISTING GROUND

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![](_page_32_Figure_0.jpeg)

![](_page_33_Picture_0.jpeg)

Page 1 of 3

# Photoionization Detector Field Screening Procedure

# **PID Calibration and Calibration Log**

All PID assays will be completed on-site using a minimum 10.2 electron volt (eV) unit. Prior to the collection and screening of samples, complete the following:

- Calibrate the PID unit to a benzene equivalent (e.g. 100 ppm isobutylene) in accordance with the manufacturer's instructions
- Perform calibrations each day the instrument is in use. Calibrate the instrument on-site and whenever significant climatic changes occur during screening activities
- Maintain an instrument log book, which may be reviewed by the DEC SMS upon request. Record the following:
  - PID make and model
  - The date and time of the calibration
  - Type of calibration gas used
  - Weather conditions including: relative humidity, wind, temperature, sample locations, background air and empty container values, and any other relevant information

# **PID Monitoring Procedures for Excavation Work**

During excavations, ambient airspace will be continually monitored with a PID for health and safety purposes as well as acquiring a background ambient air reading. The ambient air reading will be collected away from overt sources of VOCs including but not limited to excavation equipment, construction materials, and indelible markers.

Material being excavated, moved, or disturbed will be screened directly with the PID:

- In areas with no evidence of gross contamination or of suspected contamination, approximately 10% of soil being disturbed or excavated will be subject to field screening within the bucket of the excavator (e.g. one out of every ten excavator bucketfulls will be PID-screened).
- In areas of suspected contamination or with visual and olfactory evidence of contamination, <u>each</u> excavator bucket will be screened with a PID.

PID screening of material will consist of creating a narrow linear depression in the soil contained within the excavator bucket with a clean implement or a clean nitrile-gloved hand. The PID probe will be inserted into and moved along the depression for a continuous headspace reading while a clean nitrile gloved hand is cupped over the top of the depression and moved along with the PID probe. The most elevated reading will be recorded along with soil characteristics including depth, lateral location, time of screening, maximum PID

![](_page_34_Picture_0.jpeg)

reading, color, texture, moisture content, and olfactory observation. Areas of elevated PID screen readings (>10 ppm above the ambient background reading) and areas of visual/olfactory evidence of contamination will be collected for headspace measurements (see "Bag or Jar Headspace Technique" section below).

Prior to collecting samples for bag or jar headspace readings, an ambient (background) concentration reading should be completed. The background sample should be taken away from any overt sources of VOCs.

Prior to sample collection, an overview screen of the soil core or excavation bucket should be completed by creating a narrow linear depression in the soil with a clean implement and slowly sweeping the PID through the depression approximately one-inch from the soil. Cup one hand over the depression and inlet of the PID and note areas of maximum readings. Collect composite samples from the entire core or bucket, in addition to discrete samples where elevated PID measurements are observed, for bag or jar headspace readings.

#### Bag or Jar Headspace Technique

Soil samples collected during soil excavation or soil boring activities will be field screened in accordance with the headspace technique outlined below:

- Jar: Half fill one clean glass jar with the sample to be analyzed. Quickly cover the open top with two sheets of clean aluminum foil and subsequently apply screw cap to tightly seal the jars. Wide-mouth or mason-type jars are preferred. Jars ranging in size from 8 ounces (approximately 250 ml) to 16 ounces (approximately 500 ml) total capacity may be used. <u>Vigorously shake jar for 15 seconds prior to development period</u>.
- Bag: Half fill one clean plastic bag with the sample to be analyzed. Quickly seal the bag. Mix soil while bag is closed to homogenize, then <u>vigorously shake jar for 15</u> seconds prior to development period.
- Allow headspace development for at least 10 minutes. Where ambient temperatures are below 32°F (0°C), headspace development should be within a heated vehicle or building. The screening will be conducted utilizing a portable photoionization detector (PID).
- Subsequent to headspace development, vigorously shake jar or bag for 15 seconds. For the jar technique, remove screw lid and expose foil seal. Quickly puncture foil seal with instrument sampling probe, to a point about one-half of the headspace depth. For the bag technique, open a small section of the bag and insert PID inlet tube to a point about one-half of the headspace depth. Exercise care to avoid uptake of water droplets or soil particles.
- Following probe insertion through foil seal or zip seal, record highest meter response as the jar headspace concentration. Maximum response should occur between 2 and 5 seconds. Erratic meter response may occur at high organic vapor concentrations or conditions of elevated headspace moisture. If this condition develops due to high

![](_page_35_Picture_0.jpeg)

organic concentrations, the concentration should be recorded as being greater than the concentration at which the erratic response began. If it is believed that headspace moisture interfered with the results, as indicated by soil visual or textural observations, a water filter should be placed on the end of the PID and an additional sample should be collected and field screened.

Allow PID to return to ambient concentrations prior to completing subsequent measurements. If PID does not return to ambient concentrations recalibration or cleaning of the unit may be necessary.

# Adapted from:

Vermont Department of Environmental Conservation (DEC) Investigation and Remediation of Contaminated Properties Procedure (IROCPP), April 2012.

Massachusetts Department of Environmental Protection (DEP) Policy #WSC-94-400, "Interim Remediation Waste Management Policy for Petroleum Contaminated Soils"

![](_page_36_Picture_0.jpeg)

Soil Sample Collection and Decontamination Procedures

# **Soil Sample Collection**

Soil samples collected for laboratory analyses will be collected using appropriate sample containers, as provided by the receiving laboratory. Precleaned containers shall be requested from the laboratory that meet the requirements in "Specifications and Guidance for Contaminant-Free Sample Containers", EPA540/R-93/051, PB93-963316, December 1992. Prior to sampling, all sampling utensils shall be decontaminated in accordance with the procedures outlined in the section to follow, "Decontamination Procedures".

Samples obtained for volatile organic compound (VOC) toxicity characteristic leaching procedure (TCLP) analysis will be collected as grab samples in 4 ounce wide-mouth clear glass jars with teflon septa lids, or in bottles provided by the accepting laboratory. Samples will be collected in a manner to limit VOC losses; for example, no mixing of the VOC soil sample will occur and minimum air exposure will be permitted. VOC samples will be collected first followed by the sampling for additional analyses. Refer to the following section titled "Soil Sample Collection for Total VOCs and TPH-GRO via USEPA Method 8260/5035" for information regarding sampling of total VOCs and TPH-GRO

Soil samples collected for additional analyses (non-VOC) will be collected in bottles provided by the accepting laboratory. Preservation for soil samples will include placement on ice in a cooler for shipment to the laboratory.

During all soil sampling, the following general procedures will be followed:

- Field screening and visual inspection to identify the soil to be collected for laboratory analyses;
- Obtain the most representative, homogeneous sample as possible. If collecting for VOCs, minimize soil disturbance to limit VOC losses. All sampling tools will be pre-cleaned stainless steel. As appropriate, soil samples will be composited in clean stainless steel bowls;
- 7 Remove all large stones from the soil sample (greater than 1/4-inch);
- Place the sample into the laboratory-supplied container. Sample shall be packed as tightly as possible to remove air pockets;

![](_page_37_Picture_0.jpeg)

- Clean threads of jar and place teflon lid on tightly. Care shall be taken not to trap soil grains within the threads of the jar and lid;
- Zabel and preserve the sample as discussed in the section "Sample Handling, Documentation and Chain-of-Custody requirements";
- 7 Discard outer protective gloves between each sample event; and
- 7 Decontaminate samples tools as described in the section, "Decontamination Procedures".

# Soil Sample Collection for Total VOCs via USEPA Method 8260/5035

Samples obtained for total VOC or TPH-GRO analysis will be collected as grab samples in 40 mL methanol preserve vials. Methanol shall be pre-weighed from the laboratory. Between 5 to 25 grams of soil should be collected. The desired ratio of grams soil/mL methanol is 1:1, within a tolerance of +/-25%, however, the soil must be completely immersed in methanol. An additional sample of (unpreserved) soil must be collected to allow for a determination of moisture content, and the normalization of data to a dry-weight basis. Samples will be collected in a manner to limit VOC losses; for example, no mixing of the VOC soil sample will occur and minimum air exposure will be permitted. VOC samples will be collected first followed by the sampling for additional analysis. The collection procedure will be as described below as transcribed from Endyne, Inc. Laboratory Services instructions.

# Collection of Samples for Analysis

Soil Sampling for total VOCs will be as follows:

- 1. Inspect the 40 mL methanol preserve vial. Each vial will contain a five character identification number which will correspond to a specific weight of methanol as prepared by the laboratory (approximately 10 mL of methanol). Each vial also contains a line indicating the initial meniscus of the methanol. Ensure that the line matches the methanol meniscus. If they do not match, do not use that vial.
- Collect approximately 10 grams of soil, which typically corresponds to <sup>3</sup>/<sub>4</sub> to one inch of soil.
- 3. No soil should be left on the outside of the vial, the threads of the screw, or the screw to cap. Add the soil so that no methanol is splashed out of the container. If methanol is lost during the sampling, the analysis will not be accurate. In this instance, discard the vial and use a new one. At this point, return to bullet number 1 and repeat the soil collection procedure.
- 4. Screw the cap onto the vial and check that the seal is secure. Swirl the methanol inside the vial so that the methanol covers the top of the soil. Mark the new meniscus with a permanent marker.

![](_page_38_Picture_0.jpeg)

- 5. Using a four ounce or larger pre-cleaned, non-preserved glass jar, fill the jar to the top (a plastic syringe need not be used) using a pre-cleaned or disposable scoop. Ensure that the threads of the jar and cap are free of soil prior to screwing on the cap. This non-preserved sample will be submitted to the laboratory for moisture determination. This jar shall have the same sample identification number as the methanol preserved vial it corresponds to.
- 6. If possible, the samples shall be chilled to 4° C before packing them in the cooler.

Vials shall be wrapped in bubble wrap to ensure that they do not break during transportation. Ice packs or bagged ice shall be placed in between and on top of all samples after they are placed in a cooler. The temperature within the cooler shall be maintained at 4 degrees C. If not stored in a refrigerator dedicated to the storage of samples, all samples will be picked up or delivered to the laboratory within 24-hours of their collection.

#### **Soil Sample Preservation**

Samples will be collected in pre-cleaned glass containers and stored in cool conditions (approximately 4°C). After collection, samples will be promptly placed in a cooler with ice packs to preserve the samples; no chemical preservative will be added. Samples will be submitted on the same day of collection to a Vermont-certified laboratory for chemical analysis. The samples will remain refrigerated at the laboratory until analysis.

#### **Decontamination Procedures**

The method of choice for decontamination should be that which most fully removes site contaminants from the sampling equipment with least interference to the ultimate chemical analysis. Site and weather conditions frequently impose constraints upon the preferred method. Excavation contractor will be responsible for decontaminating excavation equipment.

The general decontamination methods and compounds that can be used are as follows:

- Equipment to be utilized in the collection of samples for metals analysis should be cleaned by the following steps:
  - 1. Wash equipment with a non-phosphate detergent solution (e.g. Alconox) and a brush.
  - 2. Rinse thoroughly with tap water.
- Equipment to be used for collection of samples for TPH, oil identification, and oil and grease analyses should be cleaned by the following steps:

![](_page_39_Picture_0.jpeg)

- Wash equipment with a non-phosphate detergent-solution (e.g. Alconox) and a brush.
- 2. Rinse with tap water.

1.

- 3. Rinse with reagent grade methanol.
- 4. Rinse thoroughly with deionized water.
- 5. Repeat this at each location.
- Equipment to be used for collection of semi-volatile organics (which include base-neutral extractables, PCBs, herbicides and pesticides) should be cleaned by the following steps:
  - 1. Wash equipment with a non-phosphate detergent-solution (e.g. Alconox) and a brush.
  - 2. Rinse with tap water.
  - 3. Rinse with technical grade acetone.
  - 4. Rinse with pesticide grade hexane.
  - 5. Rinse thoroughly with deionized water.
  - 6. Repeat this procedure at each sampling location.
- Equipment to be used for collection of samples for volatile organics analysis should be cleaned by the following steps:
  - 1. Wash equipment with a non-phosphate detergent-solution (e.g. Alconox) and a brush.
  - 2. Rinse with tap water.
  - 3. Rinse with reagent grade methanol.
  - 4. Rinse thoroughly with deionized water.
  - 5. Repeat this procedure at each location.
- **7** Steam cleaning is another acceptable technique for field decontamination.

More than one method or compound may be used in series for a particular site. In extreme cases, disposable equipment is recommended over decontamination. This is because the level of effort and costs required to adequately clean the equipment and dispose of the cleaning solutions may not be warranted.

# Adapted from:

Standard References for Monitoring Wells, The Massachusetts Department of Environemtnal Protection, DEP Publication #WSC-310-91

![](_page_40_Picture_0.jpeg)

Low Flow Groundwater Sample Collection Procedures

#### Low Flow Groundwater Sample Collection

Low Flow groundwater sampling is used to collect water samples that reflect the total mobile organic and inorganic loads transported through the subsurface under ambient flow conditions with minimal physical and chemical alterations from sampling operations. In essence, indicator parameters are monitored while using low pumping rates to determine when groundwater stabilization occurs and subsequently when sample collection may begin.

Low Flow groundwater samples will be collected in accordance to the USEPA Region 1 Low Stress (Low Flow) Purging and Sampling Procedure for the Collection of Groundwater Samples from Monitoring Wells, dated January 19, 2010.

# Equipment

#### Pumps

If the hydraulic head of the well is less than 20 feet a peristaltic pump and dedicated disposable tubing may be utilized.

If the hydraulic head of the well is greater than 20 feet an appropriately sized stainless steel low-flow submersible pump equipped with disposable or dedicated tubing will be utilized. Geo-subs, Grundfos pumps or bladder pumps are appropriate examples of submersible pumps.

The pumps will be run off of a power source. Usually, peristaltic pumps will require a battery pack or car battery while submersible pumps may require a generator.

It is important to note in the field notebook which pumps are used at each well for applicability to Equipment Blank samples. Each pump will have a specific serial number.

#### <u>Tubing</u>

Tubing will be Teflon or Teflon lined polyethylene tubing (preferably ¼ inch internal diameter for peristaltic set up or 3/8 inch internal diameter for submersible pump set up). Silastic tubing

![](_page_41_Picture_0.jpeg)

will be used for the section around the rotary head of the peristaltic pump. Metal barb fittings can be used to splice lengths of tubing together. These barbs will need to be decontaminated prior to use in each well (see decontamination procedure below).

### **Water Level Indicator**

A water level probe is required to measure water levels and drawdown in the well. The water level probe should be capable of a 0.01 foot accuracy.

Alternately, an oil/water interface probe can be used if free phase product is expected. Note that oil/water interface probes are fragile instruments and should not be used for measuring total depth of a well.

A steel tape measure with a weighted plumb bob should be used to sound the total depth of the wells.

# **Monitoring Equipment**

A YSI multi-phase meter fitted with a transparent 250 mL flow-through-cell will be used. The YSI meter will be capable of measuring pH, oxidation-reduction potential (ORP), dissolved oxygen (DO), specific conductance and temperature.

Turbidity measurements will be completed with the use of a LaMotte turbidity meter. Turbidity samples will be collected from the outlet of the flow-through-cell using a T-connection barb which can be opened or closed to allow the passage of water.

The YSI and turbidity meter will be calibrated at the beginning of each day of sampling. A calibration check will be performed at the end of each day to verify that the instrument is functioning properly. In addition, calibration checks can be performed at any time during the sampling day at the samplers' discretion.

- **7** Daily calibration documentation will be recorded in the field notebook
- It is important to record in the field notebook which meters are used at each wells for applicability to calibration notes. Each meter will have a specific serial number.

# Water Level Measurements

Prior to monitoring or pumping the sampler should measure water level depth and total well depth and record in the field book. Care should be taken to minimize water column disturbance.

After the initial sampling round, total well depth can be measured annually to minimize water column disturbance, unless a 'silting' problem is apparent. Measurements of total depth will indicate whether a well is filling-in due to silt accumulation. It is recommended that subsequent

![](_page_42_Picture_0.jpeg)

total depth measurement occur after well purging/sampling to minimize water column disturbance.

#### **Installing the Pump**

For a <u>submersible pump</u>, attach the tubing to the pump head. Lower the pump head, tubing and electrical line using the safety cable, taking care to minimize water column disturbance. Lower the pump to the appropriate depth (see note below). Secure the cables and tubing to the well casing using a fastener or clip. Connect the discharge end of the tubing to the flowthrough-cell/YSI and connect the pump to the power source.

For a <u>peristaltic pump</u>, lower the tubing down the well to the appropriate depth (see note below), taking care to minimize water column disturbance. Connect the tubing to appropriately size silastic tubing which will fit the pump rotary head. Connected the discharge end of the silastic tubing to the flow-through-cell/YSI and connect the pump to the power source.

The pump head/tubing intake should be located at an <u>appropriate depth</u> that will remain underwater at all times. If the well screen interval is known, then the pump head/tubing intake should be placed in the center of the well screen interval. If the well screen interval is not known then the pump head/tubing intake should be placed 2 to 5 feet from the bottom of the well to minimize mobilization of particulates present at the bottom of the well. It is recommended that the intake depth remain the same for each well for each sampling event.

#### Purging

Start the pump at a relatively low speed and slowly increase the speed until discharge occurs. Try to match pumping rate used during previous sampling events (if known) for consistency. Adjust the pump speed until there is little to no water level drawdown (as measured with a water level meter at 5 minute intervals) and record any pumping rate adjustments.

- The pumping rate should remain constant while monitoring indicator parameters and while collecting samples
- The pump must be able to 'turn over' a flow-through-cell volume between measurements (i.e. 250 mL vessel with a pumping rate of at least 50mL/min)

Purge water will be discharged into a graduated bucket and total amount of purge water will be noted on the field sheet.

If initial purge water is silty or cloudy then disconnect from the flow-through-cell and discharge the water directly to the graduated bucket. Clean the flow-through-cell of silt or debris with deionized water. Continue to measure water levels at 5 minute intervals until the water clears, then re-connect to the flow-through-cell and continue monitoring.

![](_page_43_Picture_0.jpeg)

# **Monitoring of Indicator Parameters**

Wait for the flow-through-cell to completely fill. When discharge occurs from the cell, begin monitoring indicator parameters at 5 minute intervals. Stabilization of the parameters is considered to have occurred once the change between 2 consecutive readings is within the limits in the table below:

Indicator Parameter	Units	Stabilization
Temperature	°C	3% *
рН	s.u.	±0.1 s.u.
Specific Conductance	mS/cm	3% *
DO	mg/L	10% *
ORP	mV	±10 mV
Turbidity	NTU	10% *
* Denotes percent change betweer	current reading and p	revious reading.

If after 2 hours of purging indicator parameters have not stabilized, samples will be collected but data will need to be qualified and noted that stabilization did not occur.

If the flow-through-cell needs to be cleaned during purging, continue pumping and disconnect the cell for cleaning, then reconnect after cleaning and continue monitoring. Record cleaning time interval and purpose.

# **Collecting Water Samples**

Once stabilization has been attained, or the well has been purged for 2 hours, samples may be collected.

Pumps should not be removed between purging and sampling operations and the pumping rate should remain constant. While the pump is still running, disconnect the flow-through-cell and T-connector barb and collect a sample directly from the pump's tubing.

↗ Samples must<u>Not</u> be collected from the flow-through-cell outlet.

Water samples shall be preserved according to the protocol established for the specific analytical method and for specific regulatory requirements (see sub-sections below for specific analysis requirements). The laboratory should be contacted to ensure that the proper sample preparation and sample preservation measures are taken prior to receipt of sample containers.

Samples will be collected in pre-cleaned glass or plastic containers and stored in a clean cooler with ice packs to preserve the samples (approximately 4°C). Samples will be submitted on the

same day of collection to a certified laboratory for chemical analysis. The samples will remain refrigerated at the laboratory until analysis is completed.

# Collection of Groundwater Samples for Volatile Organic Analysis ("VOA")

VOA sampling is preferred through the use dedicated disposable bailers; however, pumps may be used if care is taken to avoid aeration of groundwater prior to and during pumping (low pumping rate and small diameter tubing as specified above).

- Uncap the sample bottle taking care not to touch the teflon-faced septum. If the septum is contaminated in any way, it should be replaced.
- The sample bottle should have a pre-measured amount of concentrated hydrochloric acid ("HCl") added to it by the laboratory.
- → Fill the sample vial slowly from bailer or equivalent discharge point, minimizing air entrainment. Fill to a convex meniscus but do not overflow.
- Place the teflon-faced silicone rubber septum on the convex meniscus, teflon side down, and screw cap on.
- If air bubbles are present, open the bottle, and add additional sample to eliminate air bubbles, then reseal and repeat previous step.
- If more than three attempts are made to preclude air bubbles, then a different vial should be used.

# **Collection of Groundwater Samples for Metals Analysis**

Metals samples can be analyzed for "dissolved metals" or "total metals". This is an important distinction since filtering of samples is required for "dissolved metals" analysis while it is not (non-filtered) for "total metals" analysis.

When field filtering is required a dedicated disposable filter will be used. If the water is thought to be contaminated by organic solvents, use of filter medium such as cellulose or polycarbonate must be avoided; glass fiber or teflon filters should be used. The laboratory should be advised if samples have been filtered in the field. A general outline of the sampling procedure is as follows.

- 7 Fill the sample container from sampling device or equivalent discharge point.
  - Filtering should occur at this step, if required. The dedicated disposable filter can be attached to the discharge end of the pump tubing for sample collection.
- Add sufficient 1:1 Nitric Acid to the sample to bring the pH down to 2.0 for sample preservations. Check with pH strips to ensure enough acid was used.

![](_page_45_Picture_0.jpeg)

### **Decontamination Procedure**

Decontamination of submersible pumps should occur prior to sampling the first well and the following sampling of each well, thereafter. The pump, support cable, electrical wires, fittings and water level probe should be decontaminated by:

- ↗ Flushing/Rinsing with potable water
- ↗ Flushing/Rinsing with non-phosphate detergent solution
- ↗ Flushing/Rinsing with potable water
- 7 Flushing/Rinsing with methanol or isopropyl alcohol
- 7 Flushing/Rinsing with distilled/deionized water (cannot be recycled water)

Do not\_use distilled/deionized water stored in plastic (polyethylene) containers for decontamination as the plastic will leach phthalates and may actually introduce contamination. Instead, Nalgene glass, or Teflon vessels/bottles should be used.

Decontamination solution can be pumped from buckets through the pump and can be recycled but must be periodically changed. It is recommended that detergent and alcohols be used sparingly and that water flushing be extended.

Tubing will be disposable or dedicated to a specific well and therefore, should not require decontamination.

# **QA/QC** Procedure

If volatiles (VOC or SVOC) analysis is completed <u>Trip Blank</u> samples will be required. Trip Blank samples will consist of analyte-free water (deionized water) collected in pre-cleaned containers with appropriate preservatives as required by specific regulatory requirements. The Trip Blank sample will be added to each sample cooler that contains volatiles samples and will be collected prior to sampling, taken to the sampling site and returned to the laboratory for analysis.

<u>Field Duplicates</u> will be collected to determine precision of the sampling procedure. Field Duplicates will be required from at least one monitoring well during any sampling event and up to 10% of field samples collected. Collection of samples will occur in sequence (i.e. VOC original, VOC duplicate, SVOC original, SVOC duplicate, Metals original, Metals duplicate, etc.).

If dedicated disposable tubing cannot be utilized then <u>Equipment Blanks</u> are required. The Equipment Blank will be collected to determine if the sampling pump imparts analyte carry over from well to well. Decontamination of the pump and cable should be followed in order to minimize or eliminate carry over. Equipment Blank samples will be collected by passing clean

![](_page_46_Picture_0.jpeg)

deionized water through the pump and collecting the discharge. The Equipment Blank will include the pump only as tubing will either be disposable or dedicated.

- If the pump is dedicated to the well, the Equipment Blank will be collected prior to its placement in the well.
- If the pump is used to sample multiple wells, the Equipment Blank is normally collected after sampling from contaminated wells and not after background wells. One Equipment Blank per pump set-up, per day will be required.

# **Additional Considerations**

It is recommended that low flow sampling be conducted when air temperature is above 32°F (0°C). If used below this temperature special precautions will need to be taken to prevent groundwater from freezing in the equipment. Ice formation in the flow-through-cell will cause the monitoring probes to act erratically.

If sampling occurs in direct sunlight or hot ambient air conditions, air temperature may cause groundwater in the tubing and flow-through-cell to heat up. During these conditions, the sampler will need to shade the equipment and the tubing exiting the monitoring well should be kept as short as possible.

#### Adapted from:

Low Stress (Low Flow) purging and Sampling Procedure for the Collection of Groundwater Samples from Monitoring Wells, U.S. Environmental Protection Agency Region I, EQASOP-GW 001, January 30, 2010.

Standard References for Monitoring Wells, Massachusetts Department of Environmental Protection, DEP Publication #WSC-310-91

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10	und Sufface Levation (tet):														ce fine Sand, i	race S	Silt sea	ims, trace	, [			
	Line       Biows / 6 inch Interval       Biows														) Medium, pur	ple gra	ayeu R ay to bi	rown	—/r			
	S1       SS       24       11       0       2       2       4       6       13.6       Fill       S1) Loose       SAND, sor         S2       SS       24       7       2       4       4       5       6       35.9       2       Sand, sort       Silty Clay       \$\$       \$\$       \$\$       \$\$       \$\$       2       \$\$														casionally part ce fine Sand (	ed Silty parting	y CLA`  s), we	Y, trace Si et.	lt,			
15	Sector 100       Understand       Understand </td <td>) Medium, pur</td> <td>ple gra</td> <td>ay Silty</td> <td>/ CLAY, tra</td> <td>ace</td> <td></td>														) Medium, pur	ple gra	ay Silty	/ CLAY, tra	ace			
										$\mathcal{D}$			-			\S7	) Very soft, gra	ay Silty	CLA	Y, wet.		
													-									
20		S8	SS	24	24	19	WOH	WOH	WOH	woн		36.3	-			S8	) Very soft, gra	ay Silty	CLA	r, wet.		1
													-									-
25		S9	SS	24	24	24	WOR	WOH	WOH	woн		68.9	-			S9	) Very soft, gra	ay Silty	CLA	Y, wet.		-
													1									-
													-									
		Q10	66	24	24	20	WOR	WOU	WOU	2		35.0	-			Q1	()) Very soft					-
30		510	33			29	WUR			2		-14.8-	30.5 San	dv 3251		S1	0A - Top 18":	Gray S	Silty CL	_AY, wet.		
													Grave Clay &	elly Silt		S1	0B - Bottom 6 e to coarse Sa	': Gray nd, litt	/ Silty le fine	CLAY, sor Gravel, w	ne ∫ et. ∫	]
.00-70		F																				
35	1) N	S11 Iorth	SS ina. F	24 astine	16 a. and F	34 levation	4 based on	2 survev h	3 v VHB.	5		33.1				S1	1) Medium, gr	ay CL/	AY & S	SILT, some	e (+)	
ks	2) S	Samp nts o	bling o do not	of S2, t repre	S4, and sent SF	S6 was	s not perfo ues.	ormed in a	accordance	ce with AS	STM D	1586 re	quirements (bo	rehole was	not cle	eared v	with roller bit betw	een cor	nsecutiv	e samples) a	and blow	/
Remari	3) N 4) S 5) D	amp Drille	ole S3 r adva	anced	deep ap casing	opeared to 5' dee	disturbed ep. Boreho	as if the ble was a	sampler v dvanced o	was pushi open hole	ng a pi with th	ece of g	pravel. bit for the rema	ainder of the	e boreh	nole.	ater to the Doreho	e aurin	y roller i	uit auvance.		
の  ま り	6) L	vrille	r note	ed an ii	ncrease	e in rolle	r bit resist	ance with	i rig chatt	er beginni	ng at 3	1.5' dee	ep.									
Not	es:	1) Stra 2) Wat A.C	er Level = After	Lines Re Readings coring; N	present Ap Have Beer I.R. = Not I	proximate Be Made At T Recorded.	oundary Betwee imes And Unde	en Material Ty er Conditions S	pes, Transition tated, Fluctuat	ns May Be Gra tions Of Ground	dual. dwater Ma	y Occur Du	e To Other Factors Tha	an Those Present	At The Ti	ime Meas	surements Were Made.					
		3) Sam WOR/I 4) Prop	ple Type I=Weigh ortions	e Coding: ht of Rod/ Used: Tra	A=Auger; 0 Hammer ice = 1-10%	Core; D=l	Driven; G=Grab	c; PS=Piston S 20-35%; And	ampler; SS=S = 35-50%	plit Barrel (Spli	t Spoon); :	SΓ=Shelby	Tube; Geo=GeoProbe V	v=Vane;					Bori	ng No.: G	DB-16	6(OW)
ñ		5) Stra	ification	lines repr	resent appro	oximate bour	ndary between r	naterial types,	transitions ma	y be gradual.												. /

														BOI	RIN	<b>IG</b>	LOG		I	Borir	ng No.: (	GDB-1	6(OW)
			¢	G		D		s I	Ģ	N				Middlok	rojec				I	Page	No.:	2 o	f 2
Р	Geo .0. 1	oteck Box	hnica 699	n l / Coi	nstruct	ion / Ei	p 0 nvironme	ntal Eng 123	<i>ineers an</i> 3 Shelbu	<i>d Scienti</i> : rne Rd.,	s <i>ts</i> Suite	360			Pha	ase l	B . VT		I	File 1	No.:	837-	65.1
P P	Vind hone	sor, e: 8(	VT 02-6	05089 74-20	) 33/Fax	: 802-6	674-5943	3	So. Burl Pho	lington, V ne: 802-	VT 05 652-5	403 140				bury	/, VI		(	Chec	ked By:	DT	H
Borin Fore	ng Co man:	mpa	iny:	-	TransT John L	ech Dri	lling Servi dt	ces					Туре:	Casing: Flush	Sai	mpler: SS	Date	Gro	epth El	lev.	servations	Notes	
GeoI Date	Desigi Start	n Re	p.:	-	Jacob Novem	Wimett	2013	Date	Finished <sup>.</sup>	Novem	iber 8.	2013	I.D.: Hammer Wt ·	4.0 in. 140 lbs	<u>1.3</u> 14	<u>38 in.</u> 10 lbs	▼ 11/12/13.	(	(ft) (i	ft) 52.3	In well		
N. C	oordi	nate	:	-	553170	0.9		E. Co	ordinate:	146443	35.6		Hammer Fall:	30 in.	3	0 in.	¥.						
Stati	na Si on:	111ac 32+1		vation (	(leet):	Offset:	355.6 16 ft Le	ft					Hammer Type	e: Autor	matic		¥ ¥						
	s/ft					S	Sample	Informa	tion		1		Stra	ta ntion	-		Sa	nple [	Descrip	ption	ı		
1 (ft)	g Blow	er .		ration es)	/ery ss)	(Ų)	I	Blows / 6 i	nch Interva	al	g Time (ft)	ure int (%)		puon	Symbo								Well Log
Depth	Casin	Numb	Type	Peneti (inche	Recov	Depth	0 - 6	6 - 12	12 - 18	18 - 24	Corin (min/	Moist Conte	Depth & Elevation(feet	)		Class	sification Systen	: Burmis	ster				
													San Grave	dy elly		fin	e to coarse	Sand,	little fi	ine G	Gravel, w	et.	
													(Contin	ued)									
40		S12	SS	24	2	39	3	5	5	4		17.5				S1	2) Medium	dense,	, gray	fine	GRAVE	_	
													-			an L	d fine to coa kely roller bi	t cuttir	AND, I ngs).	little	Siit, wet.		
													-										
45		S13	SS	24	18	44	2	2	4	2		11.6				S1	3) Medium	very l	loose,	gray	SILT &		
													47				avel, wet.	to coa	arse S	ANL	), little fir	ne	
	45 S13 SS 24 18 44 2 2 4 2 11.6 45 S13 SS 24 18 44 2 2 4 2 11.6 Glacial Till 3																						
50	Clay       0     S12     SS     24     2     39     3     5     5     4     17.5       0     S12     SS     24     2     39     3     5     5     4     17.5       1     1     1     1     1     1     1     1       1     1     1     1     1     1     1       1     1     1     1     1     1       1     1     1     1     1     1       1     1     1     1     1       1     1     1     1     1       1     1     1     1     1       1     1     1     1     1       1     1     1     1     1       1     1     1     1     1       1     1     1     1     1       10     1     1     1     1       10     1     1     1     1       10     1     1     1     1       10     1     1     1     1       10     1     1     1     1       10     1     1     1     1														3	S1	4) Refusal,	fractur	red fin	ne GF	RAVEL,	. Γ	
													of Explo at 49.	ration 3 ft		SOI	ossible rolle	bit cu	Sand, ittings	trace ).	e Siit, we	et.	
													-										
55																							
													-										
													-										
60																							
													-										
													-										
65																							
													-										
													-										
70																							
S	7) S 8) D 9) B	amp riller oring	ole S r note g terr	12 at 3 ed incre ninated	9' deep ease in d with s	appear roller bi plit spo	s to be er it resistan on refusa	ntirely com ce at 47' o l at appro	posed of deep on ir kimately 4	roller bit o ferred tra 9.3 feet d	cuttings nsition eep.	s. Infer s to glac	spoon to be pus al till soils.	shing piece	of gra	avel.							
Remark	10)	Upo	n cor	npletio	n, offse	et 2.5' no	orth and s	et well to	15' deep.														
		) 0	ifiar**	Line - D	anocor+ 4	monine P	ann dan - D-r	Mat-1-1 m	mos Tr	as May D- C	dual												
Note	s: 2	) Wate A.C.	er Level = After ple Tup	Readings coring; N e Coding	Have Been R. = Not F A=Anoor	Made At T Recorded.	'imes And Und	er Conditions S	Sampler SS=S	io way ne Gra lions Of Ground	dwater Ma	y Occur Du ST=Shelby	e To Other Factors Th	an Those Present V=Vape <sup>.</sup>	t At The T	Time Meas	surements Were Made.						
	V 4 5	VOR/I ) Prop	H=Weig oortions tification	ht of Rod/ Used: Tra	Hammer ce = 1-10% esent appro	; Little = 10 ximate bour	)-20%; Some = ndary between	20-35%; And material types,	= 35-50% transitions may	y be gradual.	.,,								В	oring	g No.: C	DB-16	6(OW)

Γ									Ì						BO	RIN	[ <b>G</b> ]	LOG		Bor	ing No.: <b>G</b>	DB-2	0(OW)
					Э. F	= C	) D)		) S I	G	N				I	Project	t Nar	ne		Pag	e No.:	1 0	f 1
		Geo	tacl	<b>I</b> hnica			OR	P O	R A	T E	= D D	ete		N	Aiddle	bury	WC	RS (23)		File	No.:	837-	65.1
	P W	.O. I	Box	. 699 VT (	05089	)	uon / Li	ivir onme	123	3 Shelbu So. Bur	irne Rd., lington,	Suite VT 05	360 403		Mic	ddleb	se E oury	s , VT		Che	cked By:	DT	Ή
	P	hone	e: 80	02-6	74-20	33/Fax	k: 802-0	574-5943	3	Pho	one: 802-	652-5	140		Casing:	Sam	nler:		Ground	water O	beervations		
F	orir	ng Co man:	mpa	ny:	-	John L	eonhar	dt	ces					Туре:	H.S.A.	S	SS	Date	Depth	Elev.	N	otes	
(	Geo E	Design	n Re	p.:	_	Jacob	Wimett	0012	Data	Finish a di	Novom	bor 6	2012	I.D.:	3.25 in.	1.3	8 in.	<b>T</b> 11/0/12 0:20	(ft)	(ft)	Dearberd in	- 14	
1	Jale J. Co	oordii	nate	:	-	55351	9.8	2013	E. Co	ordinate:	14643	26.4	2013	Hammer Fall:	NA	30	in.	¥ 11/6/13, 9:30 ▼ 11/6/13, 14:00	23.0	353.9	Stabilized i	n augei	ms. rs (3 hrs
	drou	nd Su	irfac	e Ele	vation (	(feet):	Offect:	358.9	<del>1</del>					Rig Type:	CME 5	50X AT	V	¥ 11/12/13, 15:3	0 7.8	351.2	In well.		
	lain		0011	00			Superior State	Sample I	nforma	tion				Strat	- <u>Auto</u>			Sampl	e Des	crintic	'n		
		ûws∕ft			_							ne		Descrip	otion	lodi		Bumpi	e Des	enput	<i></i>		Well
(e) -	(iii) iii	ng Bl	nber	9	etratio hes)	overy hes)	th (ft)	E	Blows / 6 i	nch Interv	al	ing Tii 1./ft)	sture tent (%			Syn							Log
¢	neb	Casi	Nun	Typ	Pen	Rec (inc	Dep	0 - 6	6 - 12	12 - 18	18 - 24	Cori (mir	Moi Con	Depth & Elevation(feet)			Class	ification System: Bu	rmister				
_	_		S1	SS	24	10	0	1	3	3	3			1 Fill Layer	ed 357.		S1 SIL	) Loose, black f .T, little Coal Sl	ine to ag, tra	mediu ace fin	um SAND a e Gravel,	and	
		S2     SS     24     17     2     4     4     5     6       S3     S3     SS     24     24     3     5     5														ce Organics, m	oist.	with	arav olivo	and			
_	-	S2     S2     24     17     2     4     4     5     6       Image: S3     S5     24     24     4     2     3     5     5       Image: S3     S5     24     24     4     2     3     5     5														nge layered CL	AY &	SILT,	trace fine				
┢	5	S2       S2       S2       S4       S2       S4       S5       S4 <td< td=""><td>ers (concentral</td><td>ed in</td><td>top 5"</td><td>of sample)</td><td>),  </td><td></td></td<>														ers (concentral	ed in	top 5"	of sample)	),			
		S1       S2       S2       17       2       4       4       5       6       Clay & Silt / Silty       Clay & Silt / Silty       Silt T, litt         S2       S5       24       17       2       4       4       5       6       Clay & Silt / Silty       Clay & Silt / Silty       Silt T, litt         S3       S5       24       24       4       2       3       5       5       Silt / Silty														) Stiff, light bro	wn lay	vered (	CLAY & SII	/			
-	_	S2       SS       24       17       2       4       4       5       6       Clay & Silt / Silty Clay       Sil														e light gray SIL ers (in Silt sear	T (sea ns). n	ams), f noist v	trace Organ with wet	nic			
	10	Image         Depth & Image         Image         Image <thimage< th="">         Image         Image</thimage<>														ams.	- ,,						
	-		S6	SS	24	24	10	2	2	3	4						S4 trac	) Medium, light	browi	n parte fine Sa	and, trace	<b>ΑΥ</b> ,	
																	Ro S5	ot Pinholes and	l deca	yed R	oots, moist ed Silty CL		
	15		<b>S</b> 7	SS	24	24	14	1	2	2	3		40.8	14 Silty C	lay 344.	9	tra	ce (-) fine Grav	el, tra	ce fine	e Sand, tra	ce	
0/14	15									_					-		S6	) Medium, light	brow	n occa	isionally	· _	
DT 1/1	_																par (se	ted with gray S ams), trace (-)	ilty Cl fine S	_AY, ti Sand (i	race gray S n Silt seam	Silt ns),	
D.G																	mo S7	ist. ) Medium. arav	Silty	CLAY.	trace (-) li	aht _	
NDAF	20		S8	SS	24	24	19	WOH	WOH	WOH	1						gra	y Silt lenses, m	ioist.		( trace ( ) )	Silt	
N STA																		ce (-) fine Sand	sean	IS, WE	t.	Siit, 	
DESIG														1	Ţ								
GEOL	25		S9	SS	24	24	24	WOR	WOH	WOH	2						S9	) Very soft, gra	/ Silty	CLAY	', trace fine	e to	
GPJ	_																me	dium Sand (se	ams te	o 1/8"	thick), wet	-	
ASE B	+													27 Glacial	Till 331.	96.55							
HH Y														1									
EBUR	30		S10	SS	24	4	29	8	12	22	24	-					S1 Sa	0) Dense, gray nd, little fine Gr	SILT, avel, v	some wet.	tine to coa	arse	
			S11	SS	24	24	31	12	27	43	40						S1	1) Very dense,	gray S	SILT, s	some fine t	0	
-65.1 h	-													33 Botto	m 325	9	COS	a se sand, trac	e tine	Grave	a, wet.		6000
< 837.	35													of Explor at 33.0	ation								
EMAR		1) N 2) S	orth amp	ing, E bling o	asting	, and E S4, S6	Elevation , and S1	based or 1 was not	n survey b performe	y VHB. ed in acco	ordance w	ith AS	TM D 15	86 requirements	(borehole	e was n	ot cle	ared with augers b	etween	consec	utive samples	s) and b	blow
, LL RE	marks	3) D 4) B	rillei orine	r note g tern	d an ir ninated	ncrease d witho	e in auge	er resistar spoon refu	ice begin Isal at apj	ning at 27 proximate	" at inferre	ed trans deep.	sition to	glacial till soils.									
- SM	2 E	5) In	stal	led ol	bserva	tion we	ell to bot	tom of bor	ehole. Se	et flush m	ount well	cover a	at ground	d surface.									
# UNR#	lotes	s: 2	) Strat	ification	Lines Rep	present Ap	proximate B	oundary Betwe	en Material Ty	pes, Transitio	ns May Be Gra	dual. dwater M-	w Occur De	e To Other Factore Tho	Those Dresom	t At The Ti	me Maoo	urements Were Made					
L BOF		3	A.C.	= After ple Type	coring; N e Coding:	.R. = Not A=Auger;	Recorded. C=Core; D=	Driven; G=Gra	b; PS=Piston S	Sampler; SS=S	plit Barrel (Spl	it Spoon);	ST=Shelby	Tube; Geo=GeoProbe V	=Vane;	ine fl	e ivitaS						
SMAL		4 5	) Prop ) Strat	n=weigh ortions ification	n or Kod/ Used: Tra lines repr	ce = 1-10% csent appr	%; Little = 10 oximate bou	-20%; Some = ndary between	20-35%; And material types,	= 35-50% transitions ma	y be gradual.									Bori	ng No.: <b>G</b> l	DB-20	(OW)

Γ														BOF	RIN	I <b>G</b> ] t Nat	LOG		Bo	ring No.:	RR-1(	(OW)
	Geo P.O. Wind Phon	oteci Box Isor,	( hnica 699 VT ( 02-6	<b>5</b> N 1/Co 05089 74-20	$E_{C}$	R     R     tion / Ei	P O	R A ntal Eng 123	<b>G</b> <i>T</i> E <i>ineers an</i> 3 Shelbu So. Bur Pho	<b>N</b> ad Scienti true Rd., lington, ' one' 802-	<i>sts</i> Suite VT 05- 652-5	360 403 140	Ν	/iddleb Bridg Mid	oury les 2 dlet	WC 2 an	CRS (23) nd 102 /, VT		Pag File Che	ge No.: e No.: ecked By:	<u>1 o</u> <u>837</u> AJ	<u>f 1</u> _65 JB
Во	ring Co	ompa	iny:	/4-20	Trans	Fech Dril	lling Servi	ces	1 110		0020	110		Casing:	San	npler:		Ground	water C	Observations		
For	eman	:	5	-	James	Burrow	bridge						Туре:	H.S.A.	8	SS	Date	Depth	Elev.		Notes	
Ge	Desig	gn Re	p.:	-	Joshu	a Gilma	n	Dete	F1.1.1.1	Marah	10.00	10	I.D.:	3.25 in.	1.3	8 in.	<b>-</b> 04040.000	(π)	(π)			
Da N.	Coord	linate	:	-	55289	6.9731	5	E. Co	ordinate:	14645	66.734	13	Hammer Fall:	NA	30	) in.	¥ 3/19/13, 9:00 ¥ 3/27/13, 9:30	1.2	349.1	In well	e	
Gro	ound S	Surfac	e Ele	vation	(feet):		353.0	5					Rig Type:	CME 55	0X AT	V	¥ 3/28/13, 8:45	1.2	351.9	In well		
Sta	tion:	19+	00			Offset:	0 ft						Hammer/Rod T	Type: Autor	natic		<b>▼</b> 5/1/13, 8:10 <b>▼</b> 10/30/13, 11:	1.4	351.7	In well		
	s/ft					S	ample l	nforma	tion				Strat	a			<ul> <li>▼ 10/30/13, 11:</li> <li>▼ 11/12/13, 16:</li> </ul>	30 1.5	351.6	In well		
(ţ)	Blow			ion	8	(j)		) 		-1	Time	e (%)	Descrip	non	ymbo		¥					
epth (	Ising	Imbei	pe	netra	cove)	spth (		Slows / 0 I			oring in./ft	oistur	Depth &		s		Samp	le Des	criptio	on		Inclino.
ŭ	Ű	ź	T,	e E	R. E.	ă	0 - 6	6 - 12	12 - 18	18 - 24	йĘ	ŬŬ	Elevation(feet)	et		Class	sification System: Bu	irmister				24 24
													Dana	E	$\bigotimes$							
	-	S1	SS	24	10	2	6	12	13	7			2 Clay &	<u>.</u> Silt 351.1	翻		: Medium dens	e, dar	k brov	vn fine to		
┢													_	,		CO Gr	arse SAND, so avel, moist	ne Cla	ayey S	Silt, trace	fine	KOI KO
ł	;	S2	SS	24	16	4	2	3	5	6			1			S2 coa	: Stiff, gray CL arse Sand, trac	AY & S e fine	SILT, Grave	some fine el, wet.	e to	
		S3	SS	24	6	6	3	3	3	4				X		S3 coa	: Medium, gray arse SAND, tra	CLAN ce fine	/ & SI e Grav	LT and fir vel, wet.	ne to	
		S4	SS	24	12	8	4	8	7	6						S4	: Very stiff, bro	wn CL	AY &	SILT and	l fine	
1(													10			10						
													of Explor	m 343.1 ation								
4													at 10.0	) ft								
1/6/1																						
100. GDT	;									2												
SN ST																						
DESIG																						
0 20	1																					
6																						
(23).0																						
CRS																						
RY M		-																				
	<u>'</u>																					
MIDD																						
37-65																						
NT 8:																						
й З																						
ALL REMAR Remarks	1) S esti 2) A 3) E 4) N	Static imate All sa Explo Monif	on and ed fro imple iratior toring	d offse m a to s scre termi well ii	t showi pograp ened in nated a nstalled	n are ba hic site the fiele at 10 fee I to botto	sed on ta plan provi d using ar t with no om of bore	ped meas ded by VI n lon Scie refusal. ehole, wit	surements HB. nce Phoc h PVC co	s made in heck Moo ver flush v	the fiel del 100 with adj	d by Ge 0 PID ca jacent ti	oDesign person Ilibrated onsite t es.	nel from st o a 100 pp	ationii m isol	ng ma butylei	arked in the field by ne standard.	VHB. C	Ground	surface elev	ation sho	wn is
I I			,																			
No No	ies:	<ol> <li>Stra</li> <li>Wat</li> <li>A.C.</li> <li>Sam</li> </ol>	tification er Level = After ple Type	Lines Re Readings coring; N e Coding:	present Ap Have Beer I.R. = Not I A=Auger; 0	proximate B n Made At T Recorded. C=Core; D=	oundary Betwe imes And Und Driven; G=Gra	en Material Ty er Conditions S b; PS=Piston S	/pes, Transition Stated, Fluctua Sampler, SS=S	ns May Be Gra tions Of Groun plit Barrel (Spl	ndual. ndwater Ma it Spoon); :	y Occur Du ST=Shelby '	e To Other Factors Than Fube; Geo=GeoProbe V	Those Present	At The T	ime Meas	surements Were Made.					
ADDIT		WOR/I 4) Prop 5) Stra	H=Weigh oortions	nt of Rod/ Used: Tra lines repr	Hammer ce = 1-10% resent appro	%; Little = 10 oximate bour	-20%; Some = ndary between	20-35%; And material types,	= 35-50% transitions ma	y be gradual.									Bori	ng No. <b>R</b>	R-1(0	W)

														BOF	RIN	GI	LOG		Bor	ing No.:	RR-11	I(OW
	G P.C Win Pho	<i>Geotec</i> D. Bo	<i>chnic</i> x 699	G I I N al / Co 9 05089	= C	R tion / Er	P O	R A ntal Eng 123	<b>G</b> <i>ineers an</i> 3 Shelbu So. Bur Pho	<b>N</b> <i>ad Scientis</i> true Rd., lington, V	sts Suite VT 05	360 403	N	/iddleb Bridg Mid	oury Jes 2 Idleb	WC 2 and 2 ury	ne CRS (23) d 102 c, VT		Pag File Che	e No.: No.: ccked By	1 c 837 :A	o <u>f 1</u> 7-65 JB
В	oring	Com	502-0	5/4-20	Trans	C: 802-0	llina Servi	ces	III	JIE. 802-	052-5	140		Casing:	Sam	npler:		Ground	water O	bservations		
F	orema	un:	any.	-	James	Burrow	/bridge	000					Туре:	H.S.A.	s	S	Date	Depth	Elev.		Notes	
G	eoDes	sign R	ep.:	-	Joshu	a Gilma	n						I.D.:	3.25 in.	1.38	8 in.		(ft)	(ft)			
D	ate St	arted		-	March	21, 201	3	Date	Finished:	March	21, 20	13	Hammer Wt.:	NA		) lbs	▼ 3/21/13, 10:25	4.0	346.5	Wet samp	le (perche	ed)
N G	. Coo	rdinat Surf	e: ice El	- evation	5521t	2.9481	350 5	E. Co	ordinate:	14648	//./19		Hammer Fall:	CME 55	<u>30</u>	v v	▼ 3/21/13, 11:00	8.0	342.5	Wet samp	le	
s	ation:	11	+00	evation	(leet).	Offset:	5 ft RT						Hammer/Rod T	vpe: Autor	natic		<b>¥</b> 3/28/13, 8:15	1.2	349.3	In well		
						S	Sample I	nforma	tion				Strat	я			₮ 5/1/13, 8:15	0.9	349.6	In well		
	f)/s/m			_							ne	٩	Descrip	tion	lod		<ul> <li>▼ 10/30/13, 11:3</li> <li>▼ 11/12/13, 16:1</li> </ul>	0 0.8	349.7	In well		
( <del>0</del> )	a Bl	her		tration es)	very es)	h (ft)	E	Blows / 6 i	nch Interv	al	ng Tin /ft)	ture ent (9			Syn		C1	- D				Inclino
Dant	$\begin{array}{c c c c c c c c c c c c c c c c c c c $															Classi	Sampi ification System: Bu	e Des mister	criptio	n		Log
	$\begin{array}{c c c c c c c c c c c c c c c c c c c $															incution system: Bu	mister					
	$\begin{array}{c c c c c c c c c c c c c c c c c c c $																					
	Image:															Medium dens	e, bro	wn fin	e to coar	se		
	Image: Construction of the second															ND, some Silt, avel, moist.	some	fine to	o coarse			
	$\vec{B}$ $\vec{E}$															Very dense, b	rown	fine to	coarse	SAND		
	S1       SS       24       10       2       9       12       13       21       Fill       348.5       S1: Medium SAND, som Gravel, moi         5       S2       SS       24       9       4       6       14       39       100/6"       S2: Very de and fine to moist (wet the same same same same same same same sam															ist (wet top 3").	GRA	VEL, s	some Sill	i, ⁄		
	Image: Normal and Substrate in the second														Refusal, brow	n fine	to coa	arse SAN	ID (			
	Image: Properties of the second se														d SILT, some fi Ihtlv moist.	ne to	coarse	e Gravel,	ŀ			
	(f)       (														Refusal, brow	n fine	to coa	arse SAN	<u>اً                                     </u>	1:目:		
-	Image: Construction of the co														d SILT, some fi	ne to	coarse	e Gravel,	wet.			
	$\begin{array}{c c c c c c c c c c c c c c c c c c c $																					
4	$ \begin{array}{c c c c c c c c c c c c c c c c c c c $																					
1/6/1	S1       SS       24       10       2       9       12       13       21       Fill       348.5       S1: Mediu SAND, so Gravel, mu SAND, so Gravel, mu SAND, so Gravel, mu S2: Very C         5       S2       SS       24       9       4       6       14       39       100/6"       5       S2: Very C       and fine tc       6       6       moist (well S3: Refus       S3: Refus       S3: Refus       and SIL T,       S3: Refus       and SIL T,       S4       S5       5       8       100/5"       10       10       S4: Refus       S4: Refus       S4: Refus       S4: Refus       S4: Refus       10																					
-TGE		+		-	-																	
- DA	5	-																				
AUN/		+			<u> </u>																	
N ST/		+																				
-SIG	-	+		+																		
	20	-																				
5 - C		+																				
3).GP		1																				
SS (2:																						
WCF																						
URY	25																					
DLEE																						
MIDI																						
37-65																						
ZT 8:																						
Ê.	80																					
MAR	1	) Stat	ion ar	nd offse	t show	n are ba	sed on ta	ped meas	urements	s made in	the fie	ld by Ge	oDesign person	nel from st	tationir	ng mar	rked in the field by	VHB. G	Ground s	surface ele	vation sho	own is
L REI	2	) All s ) Drill	ampl er not	es scre ed hard	ened ir d resist	the field	d using ar auger adv	Ion Scie	nce Phoc 1 6 to 10 f	heck Mod	el 100 possib	0 PID ca	librated onsite t es/boulders).	o a 100 pp	m isob	outylen	ne standard.					
Ban	4	) Expl ) Mor	oratic itorin	on term g well i	inated a	at 10 fee to botto	t (No Refu	usal). ehole, witl	h 6-inch p	rotective f	lush m	iount co	ver.									
VLS 5		11.2	oti <sup>e</sup> · ·				ounder P ·	on Meters 17	man Ter 11	no More D. C.	dual											
N V	otes:	1) St 2) W A	auficatio ater Lev C. = Aft	ni Lines Re el Readings er corino <sup>.</sup> N	Have Bee R.R. = Not	proximate B n Made At T Recorded	imes And Unde	en material Ty er Conditions S	pes, Transition Stated, Fluctua	tions Of Ground	uuai. dwater Ma	y Occur Du	e To Other Factors Than	Those Present	At The Ti	ime Meast	urements Were Made.					
<b>I</b> TIO		3) Sa WOF	mple Ty /H=Wei	pe Coding: ight of Rod	A=Auger; /Hammer	C=Core; D=	Driven; G=Gra	b; PS=Piston S	Sampler; SS=S	plit Barrel (Spli	t Spoon);	ST=Shelby	Tube; Geo=GeoProbe V=	=Vane;					_			
ADD		4) Pr 5) St	oportion atification	s Used: Tra on lines rep	ace = 1-10% resent appr	%; Little = 10 oximate bour	0-20%; Some = ndary between	20-35%; And material types,	= 35-50% transitions ma	y be gradual.									Borii	ng No <b>R</b>	R-11(0	JW)

												BORING LOG Project Name						Bor	ring No.:	R <u>R-1</u> 3	3(OW			
	Geo P.O. Wind Phon	oteci Box Isor,	( nnica 699 VT (	<b>5</b> E N 1/Coi 05089	nstruct	<b>D</b> <b>R</b> <i>tion / Er</i>	P O	R A ntal Engi 123	G T E ineers and 3 Shelbu So. Bur Pho	<b>N</b> <i>ad Scienti</i> urne Rd., lington, V	<i>sts</i> Suite VT 05-	Middlebury WCRS (23) Bridges 2 and 102 Middlebury, VT						Pag File Che	ge No.: 2 No.: ecked By	1 ( 837 :AJB	<u>)f 1</u> 7-65 /JFW			
Bo	ring Co	ompa	nv:	/4-20.	TransT	ech Dril	lling Servi	, ces	1 110	JIC. 802-	052-5	140		Casing:	San	npler:		Ground	water C	Observations				
For	Foreman: James Burrowbridge												Туре:	H.S.A.	S	SS	Date	Depth	Elev.		Notes			
Ge	GeoDesign Rep.: Joshua Gilman											I.D.:	3.25 in.	1.3	8 in.		(ff)	(ff)						
Da N.	Date Started:         March 25, 2013         Date Finished:         March 25, 2013         I           N Coordinate:         552365,4381         E Coordinate:         1464814.311         T										Hammer Wt.: Hammer Fall:	NA	30	) in.	<b>▼</b> 3/25/13, 0:00 <b>▼</b> 5/1/13, 8:20	16.0	334.1	ln well	i tip					
Gro	ound S	urfac	e Ele	vation (	(feet):		350.1						Rig Type:	CME 55	50X AT	V	₹ 10/30/13, 13	00 1.3	348.8	In well				
Sta	tion:	13+	13			Offset:	5 ft RT						Hammer/Rod T	vpe: Auto	matic		¥ 11/12/13, 16 ▼	20 1.8	348.3	In well				
	,ff					S	ample I	nforma	tion				Strata	a tion			¥							
(t)	Blow			ion	<u>8</u> _	(f)		lesser / Circola Internel			<b>Fime</b>	e (%)	Descrip	tion	ymbo		¥							
epth (	Ising	umbe	pe	netra	scove)	spth (		slows / 0 ll			Depth &		s		Samp	le Des	criptic	Inclino.						
Ă	Ű	ź	Ty	Ρ.	an E	ă	0 - 6	6 - 12	12 - 18	18 - 24	ŬĒ	ΰŽ	Elevation(feet)	t		Class	sification System: Burmister							
_		-																						
-	-	S1	99	24	16	2	9	20	27	30			2 ¥ Fill	348.1		S1	: Dense, tan o	rav fine	e to co	arse GR	AVEL			
			00	27		-	9 29 27 39 Fill 340.1 K S1: Dense, tan gra								chips)	s) and SILT, some								
		S2	SS	24	4         5         5         6         6         7         6         7 <th7< th=""> <th7< th=""> <th7< th=""> <th7< th=""></th7<></th7<></th7<></th7<>									: Verv dense.	an fine	e to co	arse SA	ND						
	, 												and SILT, trace fine to coarse Gravel,											
		S3	SS	20	18	6	17	60	70	100/2"						 S3	: Verv dense.	an ara	v SIL	T and fine	e to	1:目:		
													]				arse SAND, so	me fin	e to c	oarse Gr	avel,			
		S4         SS         11         11         8         31         100/5"											_\of :	sample, gray a	nd dry	bottor	m half).							
10												S4: Refusal, gray SILT and fine to coarse												
																SA		U CUAI	se Gia	avei, ury.	]			
4																								
1/6/1																								
-105 		0.5	66	24	24	14	25	55	57	57 67 S5: Very dense					· Verv dense	arav Sl	ITan	d fine to		_				
	;	00	55	24	24	14	- 55	- 55	51	07						COa	arse SAND, so	me fin	e to co	oarse Gr	avel,			
AND/													<b>⊥</b>	-		ury	(spoon lip we	ι).				-		
N ST		S6	SS	0	0	16.9	50/0" <u>:</u> C	= 100%	; RQD=	51%]	4		Bedroo	<b>k 333</b> .1		∖S6	: Refusal, no r	/	=					
ESIG		101.	_C_	60	-60-	1/					5					C1: Fair quality, moderately hard, fresh to								
	)										5					joir	nting, gray and	white	banded MARBLE.					
						22					5					ho	rizontal. Strong	g react	ion to	dilute HC	XI.			
(23).6											5					~	. Oak 1			h	- 1-			
CRS	-	C2	С	60	60		[REC	= 100%	; RQD=	81%]	4					C2 clo	se to moderat	, mode e jointii	rately ng, gra	nard, fre ay and w	sn, hite			
≥	-	-									4					bai HC	nded MARBLE	. Stror	ng rēa	ction to d	ilute			
	;	-									4													
		$\left  \right $									4													
-65 N		$\vdash$											Botton	n 323.1	K//							-		
837	+												of Explora at 27.0	ation ft										
NOL 30		$\square$											1											
MLS SMALL REMARK Remarks	1) S esti 2) A 3) H 4) C	Static imate All sa HSAF Groui	on and ed fro mple R and ndwat	d offse m a to s scree SSR a ter mon	t showr pograpl ened in at 17 fe nitoring	n are ba hic site   the field et deep. well ins	sed on taj plan provi d using ar . Driller p stalled 3/2	ped meas ded by VI n lon Scie ulled auge 8/13 by a	urements HB. nce Phoc ers, spun ugering a	s made in theck Moc 4" FJ cas Idjacent to	the fiel lel 1000 ing and o explor	Id by Ge 0 PID ca d set up ration. \	eoDesign personn alibrated onsite to to core C1. Well installed to t	nel from s o a 100 pp pottom of	tationir om isot borehc	ng ma butylei ble, wi	rked in the field b ne standard. ith 6-inch protectiv	/ VHB. C	Ground :	surface ele over.	vation sh	own is		
No	es:	2) Wat A.C	er Level = After	Readings coring; N	Have Been .R. = Not I	Made At T Recorded.	imes And Unde	er Conditions S	tated, Fluctua	tions Of Groun	dwater Ma	y Occur Du	e To Other Factors Than	Those Present	At The Ti	ime Meas	surements Were Made.							
		3) Sam WOR/I	ple Type I=Weigh	e Coding:	A=Auger; C Hammer	C=Core; D=l	Driven; G=Gra	b; PS=Piston S	ampler; SS=S	plit Barrel (Spl	it Spoon); !	ST=Shelby	Гube; Geo=GeoProbe V=	Vane;					р. ·		7 404	0140		
AD		5) Stra	ification	lines repr	esent appro	oximate bour	adary between	material types,	transitions ma	y be gradual.									BOLI	ng NOK	⊼-13(I	JVV)		

Γ															BO	Boring No.: <b>RR-1</b>	6(OW				
	GEODESIGN														]	Projec		Page No.: 1	of 2		
	(	Geot	ech	I nica	¯ N l∕Coi	с ıstruci	Ο R tion / Ei	р O nvironme	R A ntal Eng	T E ineers an	∃ <b>D</b> nd Scienti	sts		N	/liddle Brid	bury		File No.: 83	7-65		
	P.0 W Ph	O. B inds	ox or, 80	699 VT ( 2-67	)5089 74-203	33/Fax	k: 802-6	574-5943	123	3 Shelbu So. Bur Pho	rne Rd., lington, one: 802-	Suite VT 05- 652-5	360 403 140		Mie	ddlel		Checked By:			
В	oring	g Cor	npar	ıy:	_	Trans	Fech Dri	lling Servi	ces						Casing:	San	npler:		Ground	water Observations	
F G	orem eoDe	an: esign	Ren	.:	_	James Joshu	<u>s Burrow</u> a Gilmai	/bridge n						Type:	H.S.A. 3.25 in.	1.3	3S 18 in.	Date	Depth (ft)	Elev. Notes (ft)	
D	Joshua Oliman         Joshua Oliman           Date Started:         March 26, 2013         Date Finished:         March 27, 2013         1												Hammer Wt.:	NA	140	0 Ibs	¥ 3/26/13, 15:30	6.0	344.4 Wet sample		
N	. Co	ordin	ate:	<b>F</b> 1	_	55260	0.271		E. Co	ordinate:	14647	18.142		Hammer Fall:	NA	30	) in.	<b>▼</b> 3/27/13, 9:20	0.0	350.4 In open hole overn	ight
S	roun tatior	a Su 1: 1	5+6	e Elev 7	ation (	ieet):	Offset:	<u>350.3</u> 6 ft RT	/					Hammer/Rod 7	CIVIE 5	omatic	v	<b>\$</b> 3/28/13, 8:20 <b>\$</b> 5/1/13, 8:30	1.6	348.5 In well	
		_					S	Sample I	nforma	tion				Strat	a			<b>¥</b> 10/30/13, 13:4	1.8	348.6 In well	
		ows/fi			<u>п</u>							me	0	Descrip	otion	lodi		¥ ¥			
49) 44		ng Bl	her	0	etratio nes)	overy ies)	th (ft)	E	Blows / 6 in	nch Interv	al	ng Ti	sture tent (9		Syn			Sample	- Des	cription	Inclino.
Dani	4	Casi	Nun	ac and a second a sec				18 - 24	Cori (mir		Depth & Elevation(feet)	feet)		Class	sification System: Bu	mister	cription	Log			
														Balla	st						
														2			01			<u> </u>	
		:	S1	SS	24	4         2         9         7         7         3         Silty         348.4									40.7	S1 SA Silt	: Medium dense ND and fine to t, moist to wet.	e, gray coars			
_	5	-	S2	SS	24	12	4	1	3	4	9					0 (	S2 SIL	2: Loose, gray fir LT, little fine Gra	ie to c avel, r	coarse SAND and noist to wet.	
		:	S3	SS	24	12	6	18	19	13	12						S3 fin	: Dense, tan fin e to coarse GRA	e to c AVEL,	oarse SAND and , little Silt, wet.	
		:	S4	ss	13	3	8	11	14	50/1"				9			S4	: Refusal, tan fi	ne to	coarse SAND and	「追い
	10													Bould	er/ 341. es	4		e to coarse GRA	AVEL,	, some Siit, wet.	<u>1:目:</u>
4			C1	С	26	26	11	[REG	C= 100%	5; RQD=	0%]	4		12 Bodro	<u>ck 220</u>		C1 Bo	I:Top 6" Boulder httom 20" <sup>.</sup> Verv r	fragr	nents. wality moderately	
1/6/1												10		Bedio	CK 330.	*	ha	rd, fresh to sligh	itly we	eathered, close	_
GDT -	_	-	C2	2 C 34 34 13.2 [REC= 100%; RQD= 12%] 5.5   jointed gray with whi LIMESTONE (upper								er 7")	grading to very								
ARD .	15			_								10						bse jointed dark ( casional thin (<	gray F 1/8" th	PHYLLITE with nick) beds of	
AND		-	СЗ	с	6	6	16	[REG	C= 100%	 ;; RQD=	0%]	10						nestone and pyr	ite ind	clusions. Fracturing	F.
LS NS			C4+	-C	-36-	-35-	-16.5-	[REC	C= 97%; 	RQD= 6	63%] <del></del> 	6					~6	5 degrees from	horizo	ontal in Phyllite	
DESIC												6					Lin	nestone portion	s with	no reaction in	
GEO	20											10-		Botto	m. 330.	.9		iyllite portions.	it	adarataly bard fraab	
WCRS (23).GPJ														at 19.5	5 ft		to joir bai LIN alc	slightly weather nted, dark gray v nds interbedded MESTONE. Frac ong Phyllite beds	ed, sh vith o PHY cturing at ~6	nattered to close ccasional white LLITE and g typically occuring 65 degrees from	
	25		+														ho Lin Ph	rizontal. Strong mestone beds w iyllite.	reacti th no	on to HCl in reaction in the	
-65 MIDE		4															C3 fre	B: Very poor qua sh to slightly we	lity, m ather with t	noderately hard, ed, shattered, dark thin (~1/8" thick)	
ONT 837	+													•			Ph	nyllite bedding. S nestone surfaces	trong s with	reaction to HCl on n no reaction on	
L REMARK F		1) St estin 2) All 3) Dr	atior nateo sar iller	n and d froi nples	l offset n a top s scree d incre	t shown bograp ened in eased a	n are ba hic site the field	sed on tap plan provi d using an inding app	ed meas ded by VI I lon Scie d rig chatt	urements HB. nce Phoc er advance	made in heck Moc	the fiel	ld by Ge 0 PID ca 9 to 11	I coDesign person alibrated onsite t feet deep (possi	inel from s to a 100 p	stationii pm isol	ng ma butyle	arked in the field by '	/HB. G	Fround surface elevation s	nown is
LS SMAL		4) HS 5) Mo	SAR	at 1 ring	1 feet ( well in	deep. [ istallec	Driller ad	Ivanced 4	" FJ casir hole, with	ig with sp n 6-inch p	in shoe a rotective	nd core flush m	ed Day 2 iount co	ver.							
N N N	otes:	1) 2) 3)	Stratif Water A.C. = Samp	ication Level After e Type	Lines Rep Readings coring; N Coding: /	Have Been R. = Not A=Auger; (	proximate B n Made At T Recorded. C=Core; D=	oundary Betwe imes And Und Driven; G=Gra	en Material Ty er Conditions S b; PS=Piston S	pes, Transition Stated, Fluctuat Sampler, SS=S	ns May Be Gra tions Of Groun plit Barrel (Spl	idual. dwater Ma it Spoon); :	ay Occur Du ST=Shelby	e To Other Factors Thar Tube; Geo=GeoProbe V	n Those Preser	it At The T	ime Meas	surements Were Made.			
ADDIT		4) 5)	OR/H Propo Stratif	Weigh rtions U	t of Rod/l Jsed: Trac lines repro	lammer ce = 1-10% esent appro	%; Little = 10 oximate bour	0-20%; Some = ndary between	20-35%; And material types,	= 35-50% transitions ma	y be gradual.									Boring NoRR-16	(WO

														BORING LOG							Boring No.: <b>RR-16(OW</b>			
			Ċ	ЭE	= 0	D	E	s I	G	N		Project Name							Page No.: <u>2 of 2</u>					
	Geo	otech	• nica	¯ N d∕Coi	c o	o R ion / Er	P O vironme	R A ntal Eng	T E	= D d Scienti:	sts		Middlebury WCRS (23) Bridges 2 and 102 Middlebury, VT							e No.: <u>83</u>	7-65			
F	P.O. I Vind	Box sor,	699 VT	05089	)			123	3 Shelbu So. Bur	rne Rd., lington, V	Suite VT 05	360 403								ecked By:	FW			
Bori	hone	e: 80	)2-6 nv:	74-20	33/Fax TransT	:: 802-6 ech Dril	574-5943 ling Servi	s ces	Pho	one: 802-	652-5	Casing	:	Sam	pler:		Ground	water C	Observations					
Fore	man:			-	James	Burrow	bridge						Type: <u>H.S.A</u> .	<u> </u>	S	S	Date	Depth	Elev.	Notes				
Geo.	Josnua Gilman         I           Date Started:         March 26, 2013         Date Finished:         March 27, 2013         I														1.38 140	8 in. ) Ibs	▼ 3/26/13, 15:30	6.0	344.4	Wet sample				
N. C	oordi	nate:		-	55260	0.271		E. Co	ordinate:	14647	18.142	Hammer Fall <u>: NA</u>		30	in.	▼ 3/27/13, 9:20	0.0	350.4	In open hole overni	ght				
Grou Stati	ınd Sı on:	ırfac 15+6	e Ele 67	vation (	feet):	Offset:	350.3 6 ft RT	7				Rig Type:CME Hammer/Rod Type: A	550 550	X AT	V	¥ 3/28/13, 8:20 ¥ 5/1/13, 8:30	1.6 1.9	348.8 348.5	In well In well					
	t					S	ample I	nforma	tion				Strata				¥ 10/30/13, 13:40	1.8	348.6	In well				
_	lows/f			ц		_					me	(%)	Description		lodu		¥ ¥							
oth (ft)	ing Bl	nber	e	etratic thes)	covery ches)	oth (ft)	E	Blows / 6 inch Interval			ing Ti n./ft)	isture itent ('	Danith &		Syr		Sample	e Des	criptio	on	Inclino.			
Def	Cas	INU	Typ	Pen (inc	Rec (inc	Der	0 - 6	6 - 12	12 - 18	18 - 24	Cor (mi	Cor Cor	Elevation(feet)			Class	ification System: Bur	mister			Log			
																C4 clo	: Fair quality, m se to moderate	odera jointir	itely h 1g, int	ard fresh, erbedded dark				
_																gra ligh	y PHYLLITE wi nt gray/ white LI	th pyr MES1	ite ind IONE	clusions and (upper 12")				
																gra bar	ding to light gra ding LIMESTO	y with NE (t	occa	asional white n 24").				
35																Fra	acturing up to ~	20 de reacti	egrees	s from HCL on				
															Lin	nestone surface	s with	n no r	eaction on					
																<u></u>								
40																								
45																								
50																								
- 50																								
55													1											
60													<u> </u>											
arks																								
Rem																								
		) Strat	ification	Lipes Do-	Tresent Area	roximate P	undary Paters	en Material T	nes Transition	15 May Ro Geo	dual													
Note	s: 2	) Wate A.C.	= After	Readings coring; N	Have Been .R. = Not F	Made At T	imes And Und	er Conditions S	rated, Fluctuat	tions Of Ground	dwater Ma	y Occur Du	e To Other Factors Than Those Pro	esent At	t The Tir	me Meas	urements Were Made.							
	3 V 4	) Samp VOR/H ) Prop	pie 1 yp I=Weig ortions	e Coding: . ht of Rod/ Used: Tra	A=Auger; C Hammer ce = 1-10%		-20%; Some =	20-35%; And	ampier; SS=S = 35-50%	рат њаттеі (Spli	spoon); S	51=Shelby	uoe; Geo=GeoProbe V=Vane;						Bori	ng No <b>RR-16</b>	ow)			
	5	) Strati	ification	lines repr	esent appro	ximate bour	ndary between	material types,	transitions ma	y be gradual.											,			